

Towards High Compression Ratios

Chau, Long Phi

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Outlines:

- **Requirements**

- **Design / Optimization Cycles**
 - Geometry
 - 5MHz Kicker
 - Single Bunch Beam Dynamics
 - Merging Scenario
 - Magnet Design
 - Beam Dynamics with Realistic Field Distributions

- **Outlook**

Outlines:

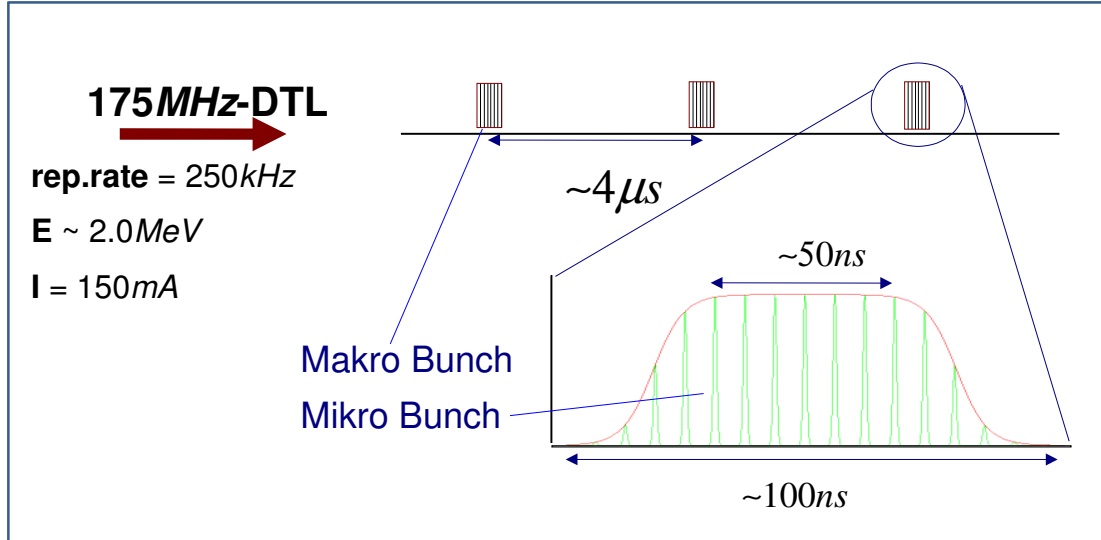
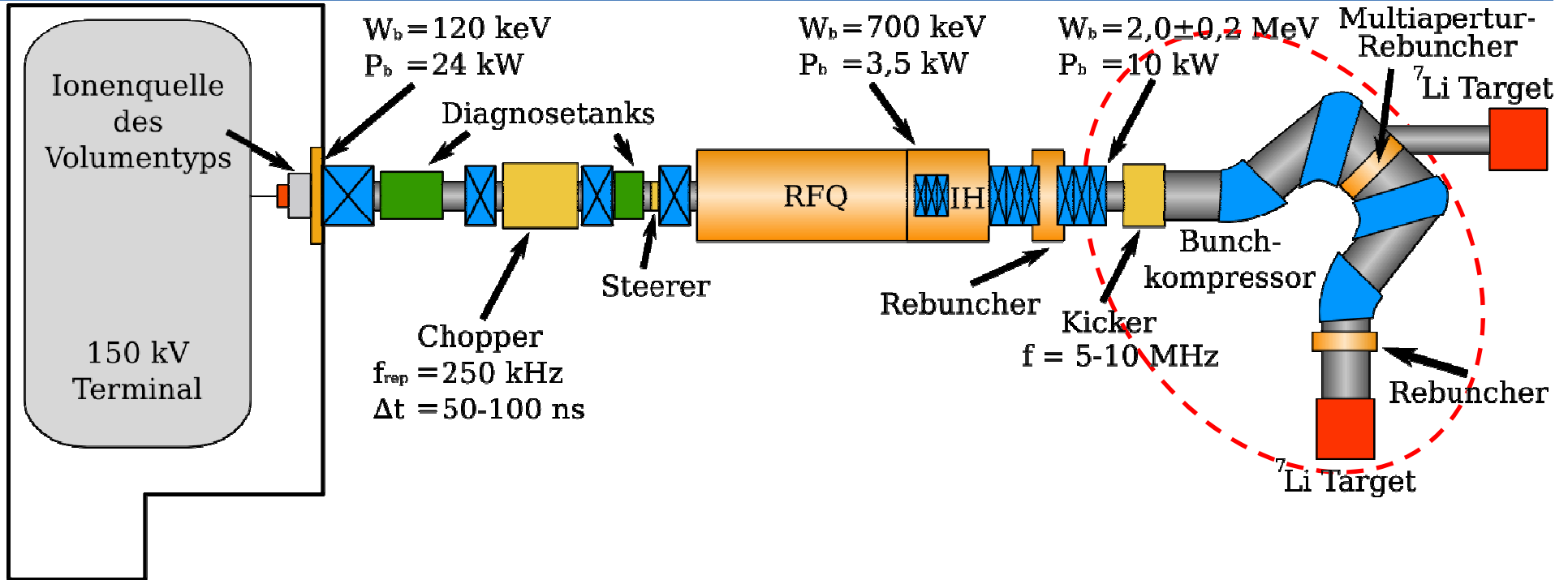
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FRANZ: Bunch Compressor - Requirement

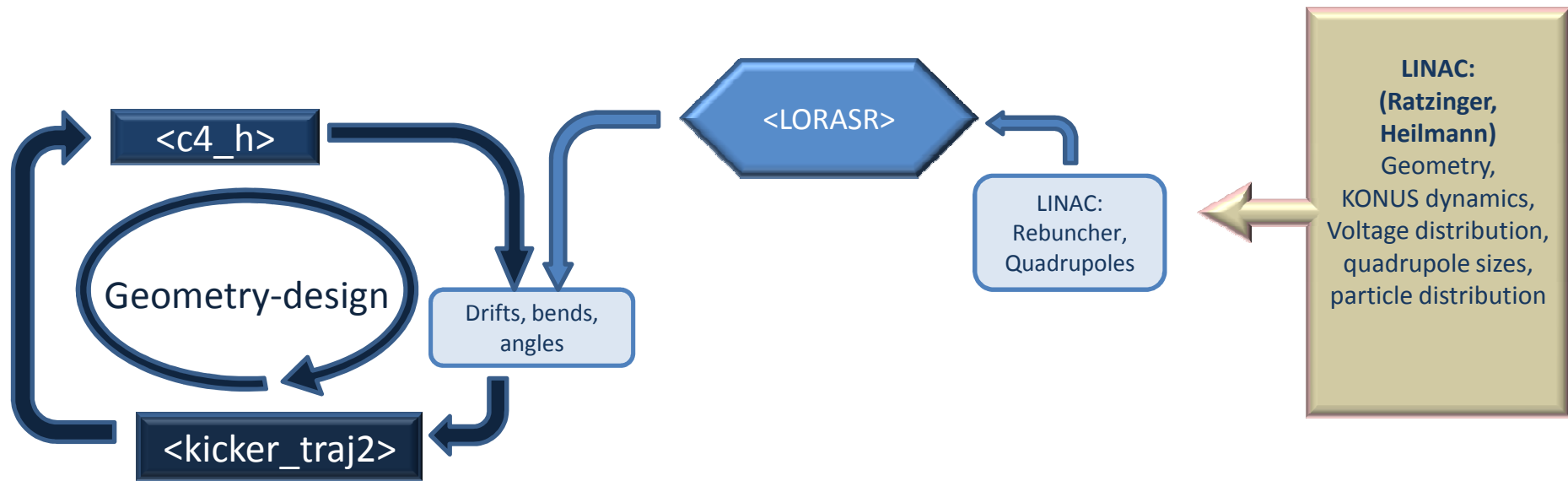


- $N_{\text{bunch}} = 9$
- $\Delta T = 50\text{-}100\text{ ns} \Rightarrow \Delta T \approx 1\text{ ns}$
- $A_{\text{(beam at target)}} < 3 \times 3\text{ cm}^2$
- $I_{\text{(per pulse)}} \approx 8\text{ A}$
- $\Delta W < \pm 5\%$

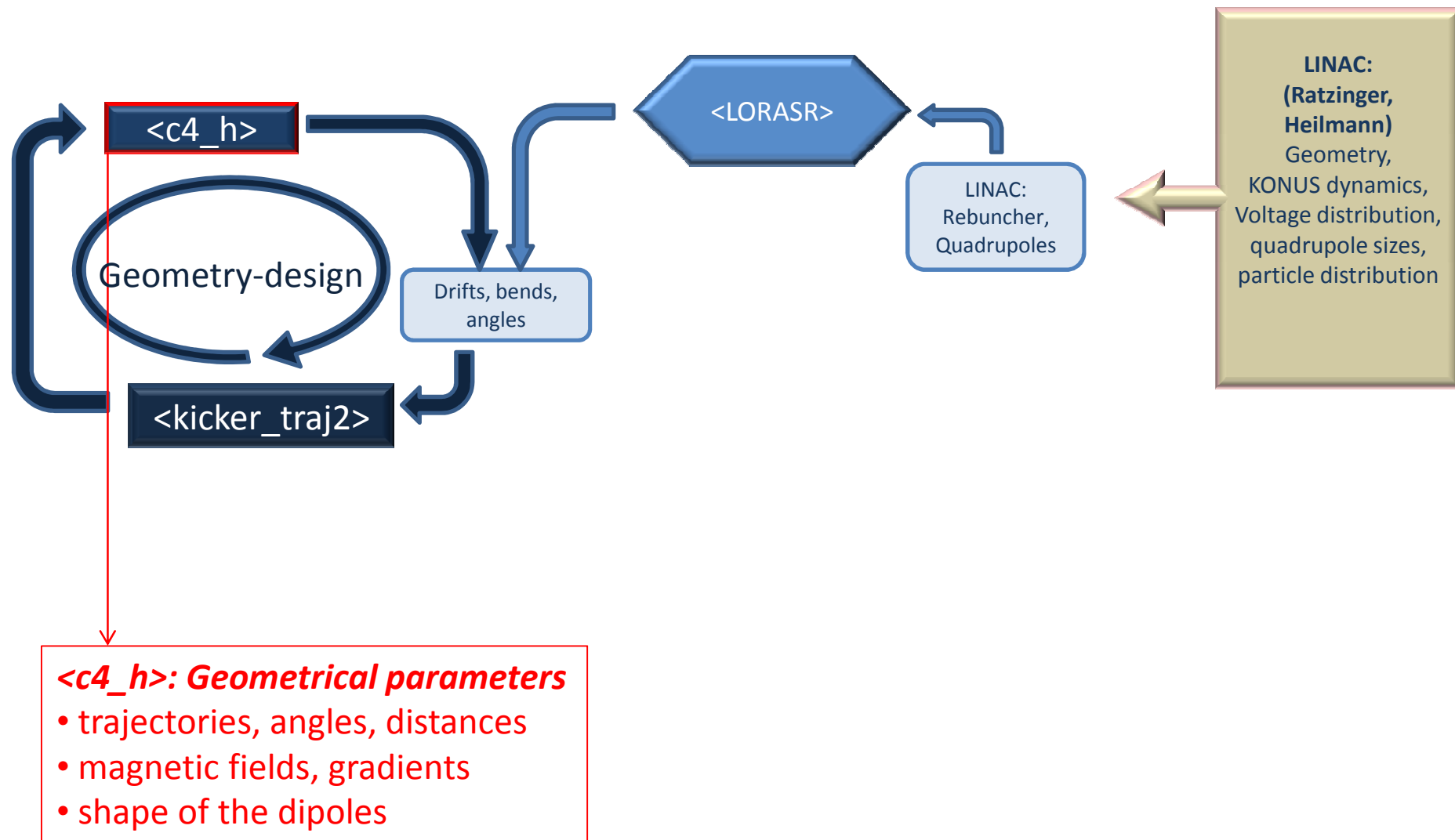
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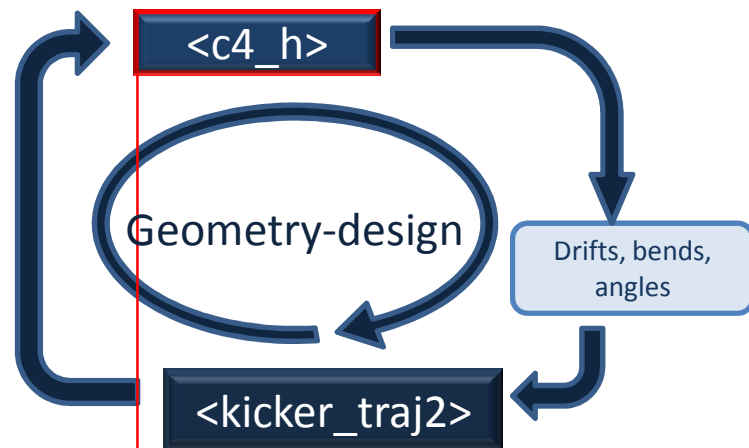
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Bunch Compressor: Design / Optimization Cycles



Bunch Compressor: Design / Optimization Cycles

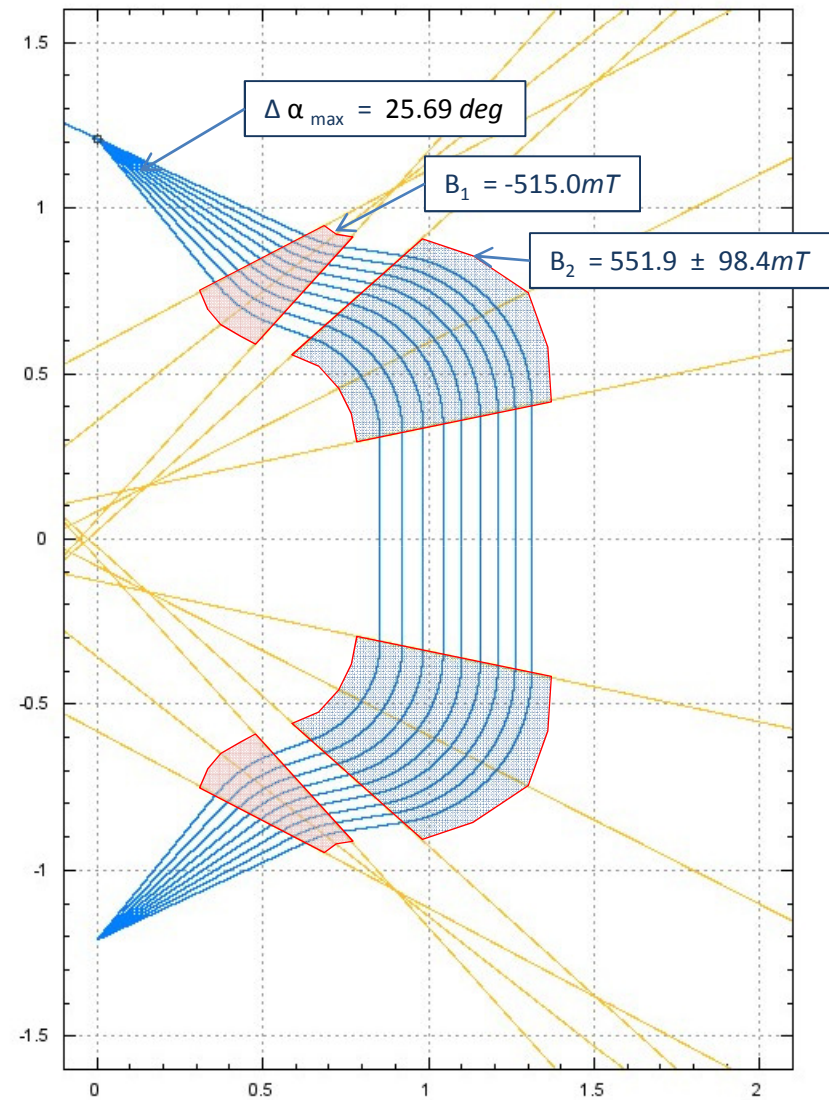




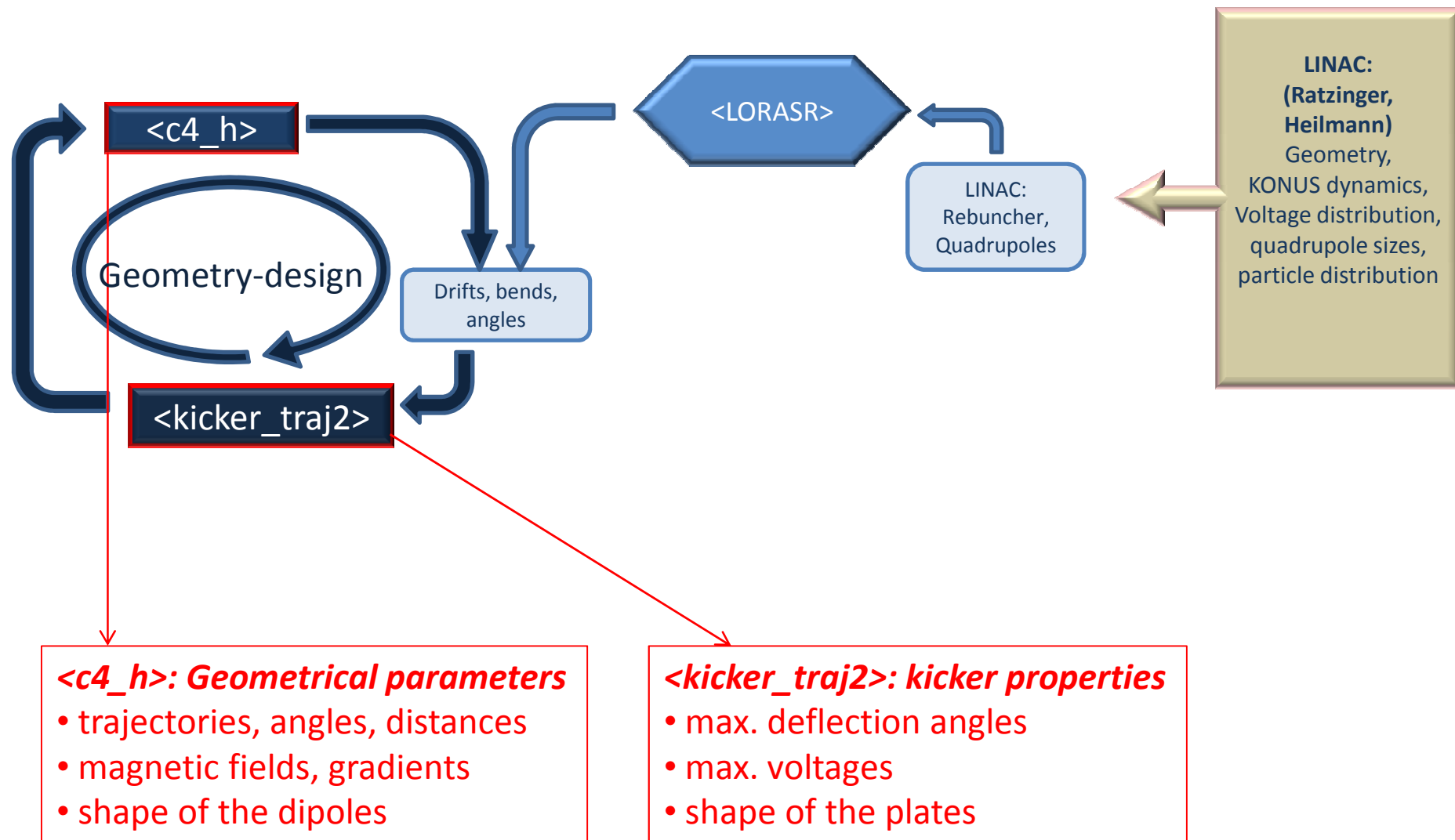
$\langle c4_h \rangle$: Geometrical parameters

- trajectories, angles, distances
- magnetic fields, gradients
- shape of the dipoles

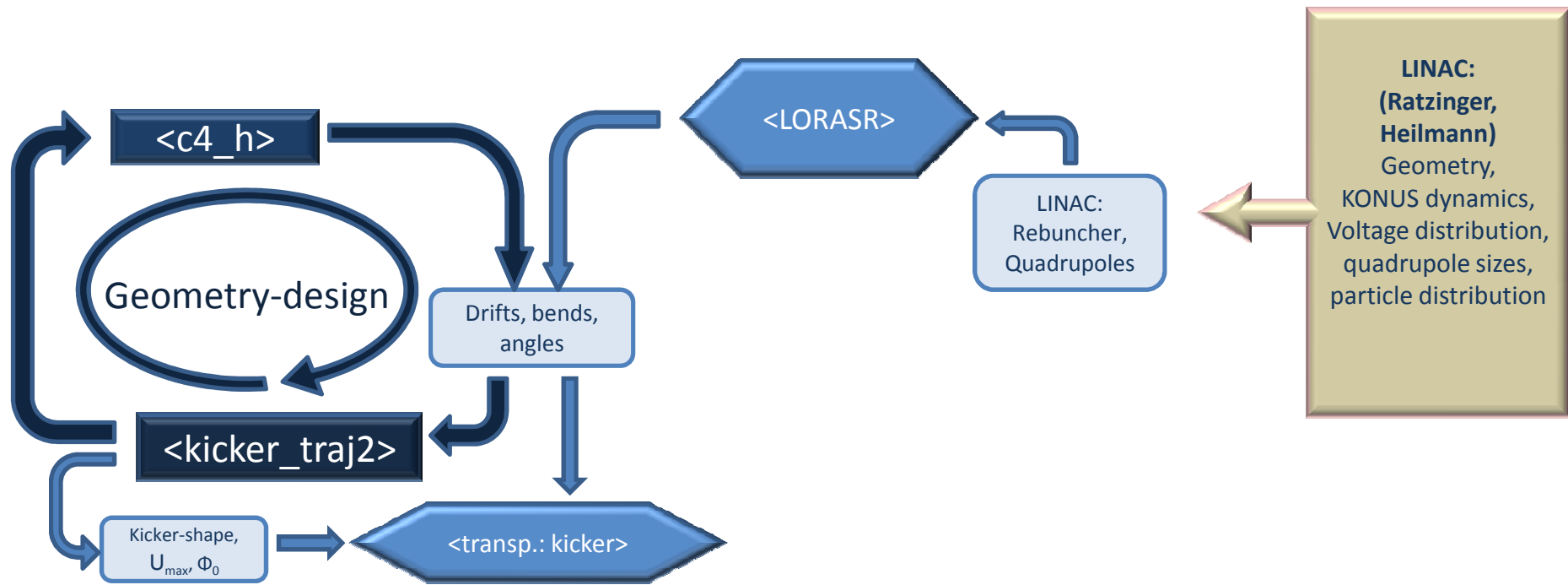
Geometry: g9_5x



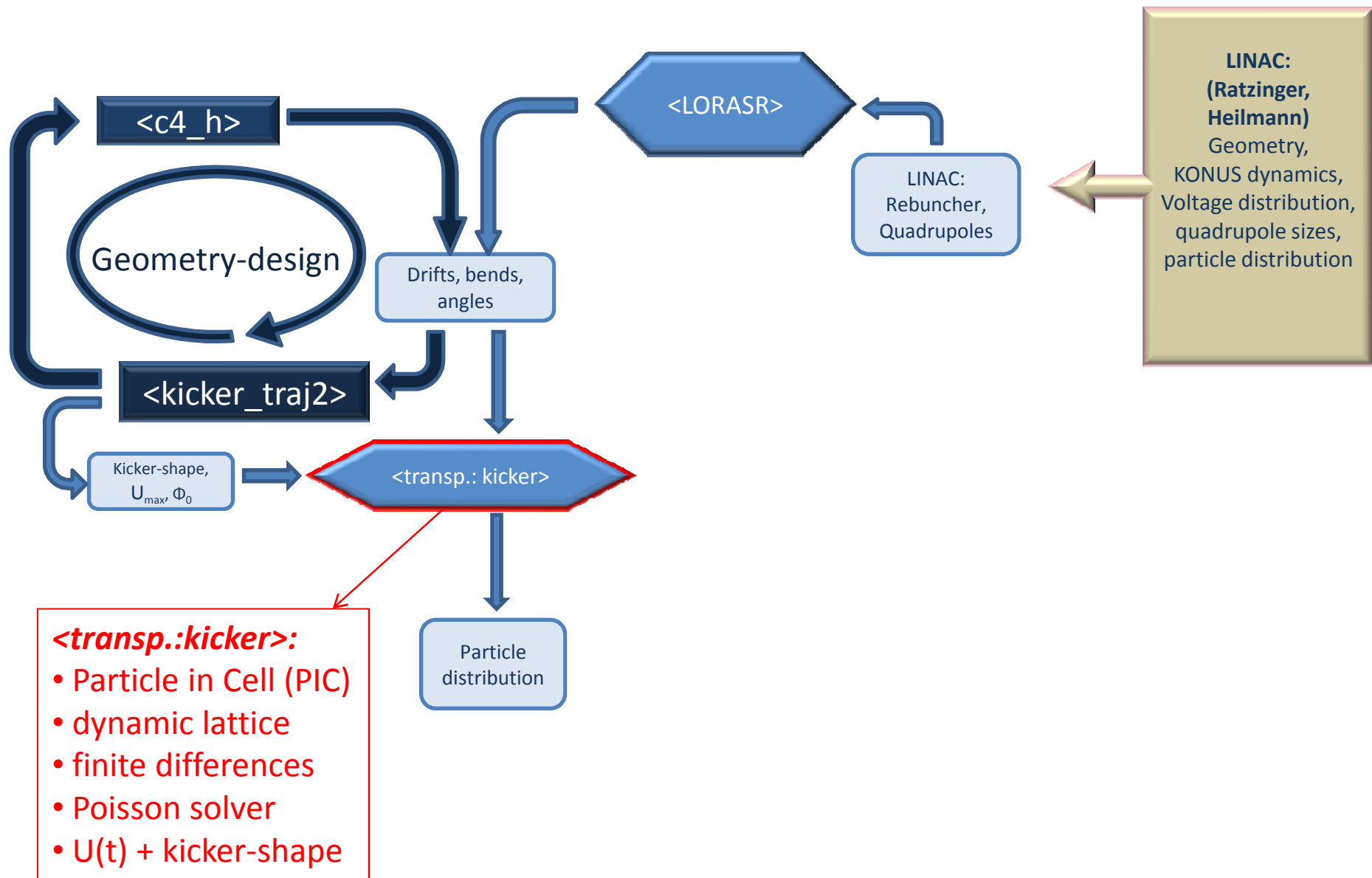
Bunch Compressor: Design / Optimization Cycles



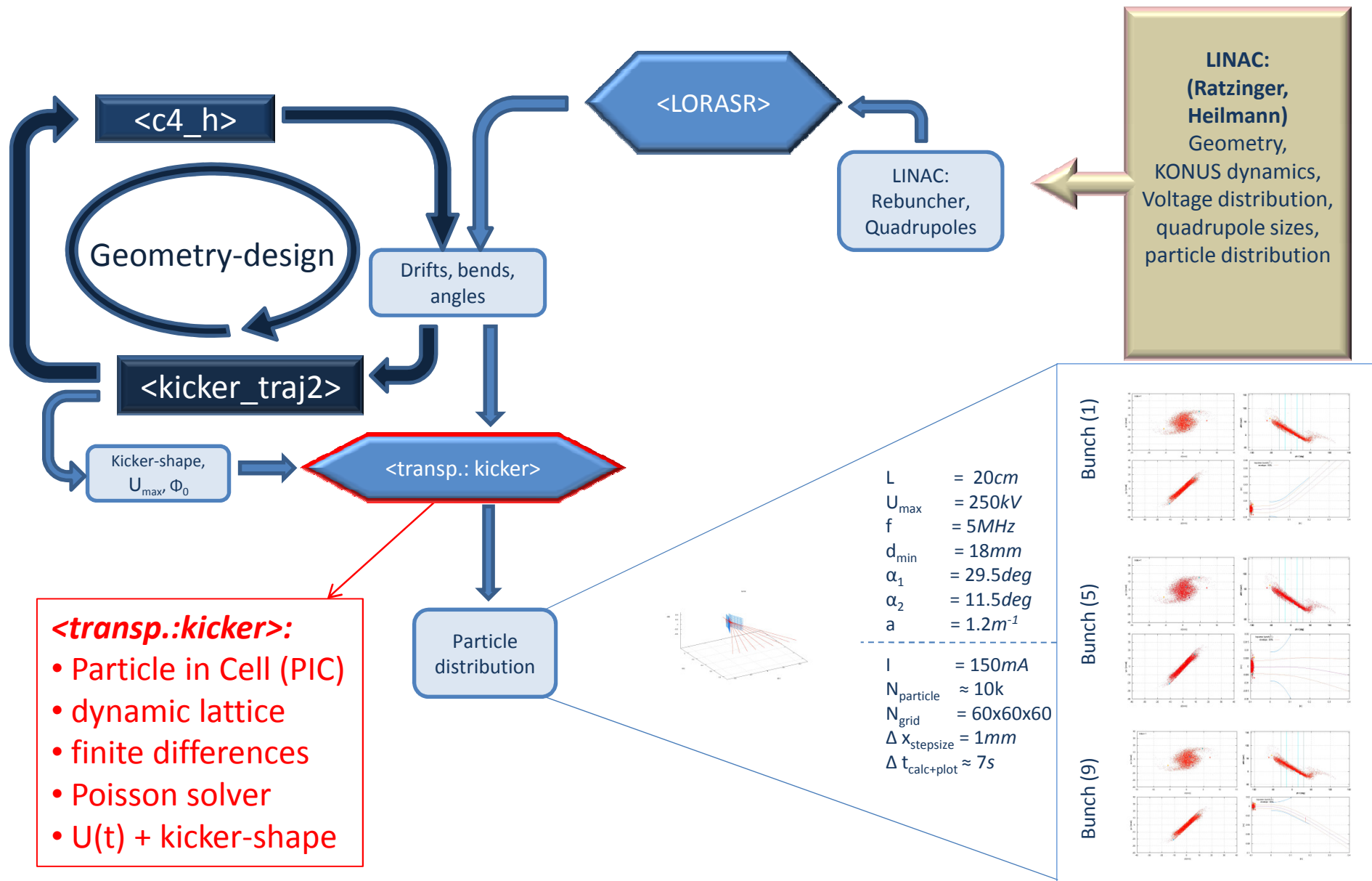
Bunch Compressor: Design / Optimization Cycles



Bunch Compressor: Design / Optimization Cycles



Bunch Compressor: Design / Optimization Cycles



Analytical estimations:

- RLC-Resonator
- Geometrical parameters:
 - diameter, lengths
 - coil geometry
 - number of windings
- Inductance L and Capacitance C
- RF-properties: f , Q_0 , P



Y. Nie

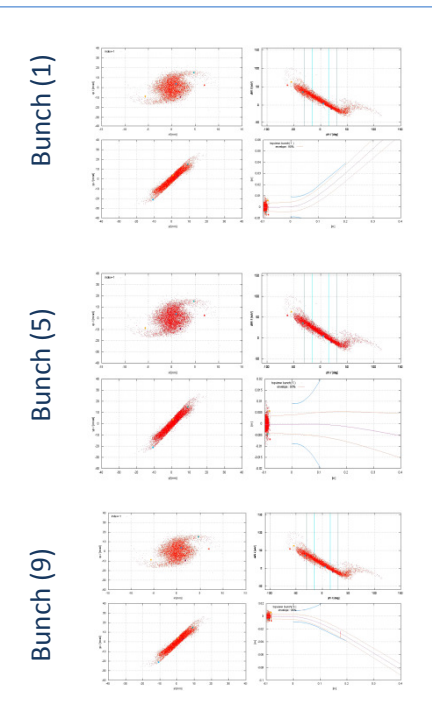
Visitor Scientist

Beijing University

(supervised by U. Ratzinger at FFM)

Technical realization?

L	=	20cm
U_{\max}	=	250kV
f	=	5MHz
d_{\min}	=	18mm
α_1	=	29.5deg
α_2	=	11.5deg
a	=	$1.2m^{-1}$
<hr/>		
I	=	150mA
N_{particle}	\approx	10k
N_{grid}	=	60x60x60
$\Delta x_{\text{stepsize}}$	=	1mm
$\Delta t_{\text{calc+plot}}$	\approx	7s



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Scaled Model (analytical):

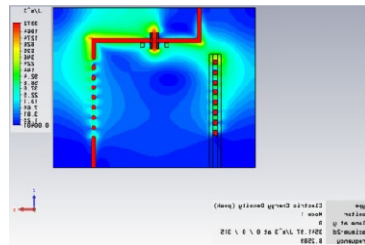
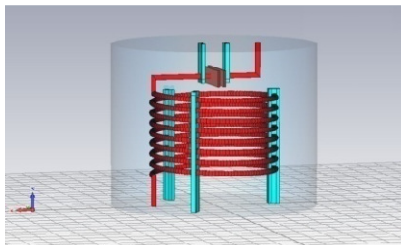
Number of turns	8	
Length of the coil	200	mm
Radius	150	mm
Effective Resistivity	0.246	Ω
Effective Inductance	12.9	μH
Effective Capacitance	28.8	pF
Frequency	9.09	MHz
Intrinsic Quality Factor	2986	
Shunt impedance	4.4	MΩ
Power losses @ 250kV	14.8	kW

Analytical estimations:

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- Geometrical parameters:
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Numerical estimation:

- 3D Cavity designs with CST Studios



Y. Nie

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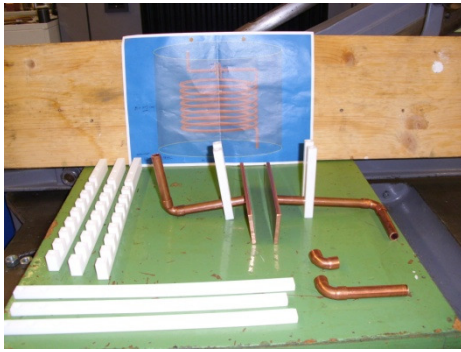
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Construction and assembly at IAP- and IKF-workshop



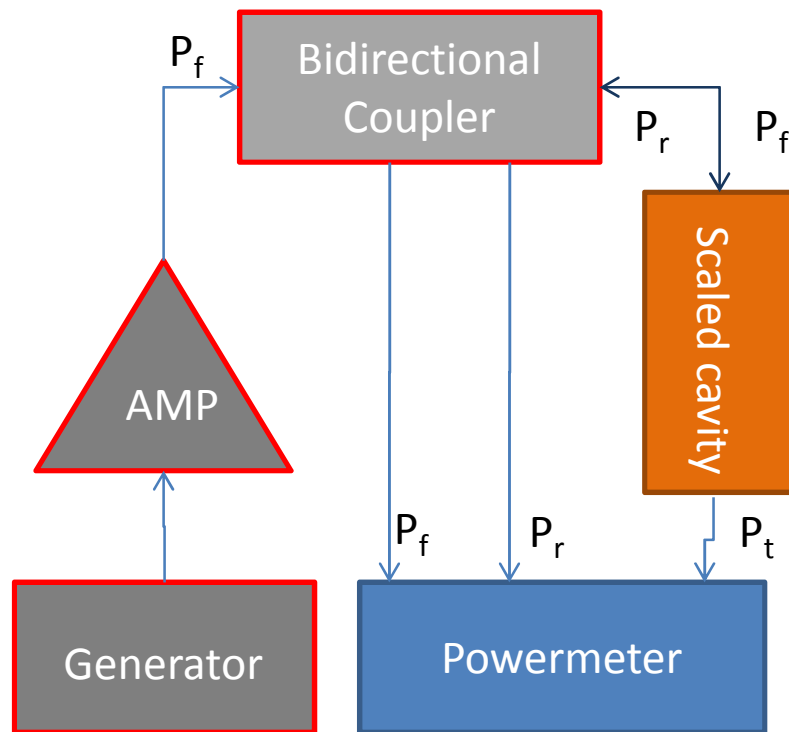
Construction and assembly at IAP- and IKF-workshop



THANKS !!!
@Workshops
@A. Schempp

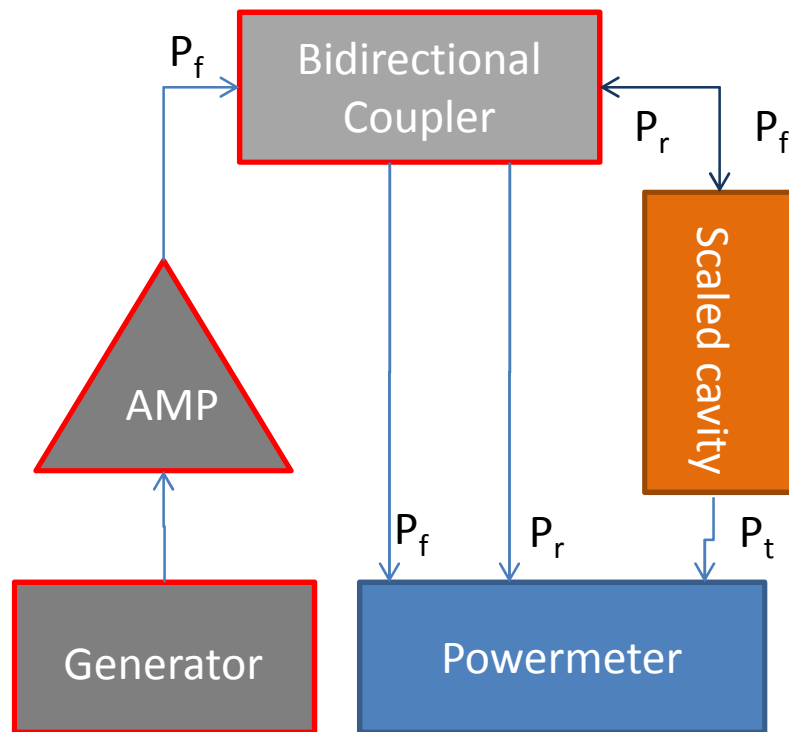


Measurements at scaled Model



THANKS to H. Podlech
for
his support and discussions!

Measurements at scaled Model



$$P_t : U(t) = U_0 \cdot \exp(-t/\tau) \sim E(t)$$

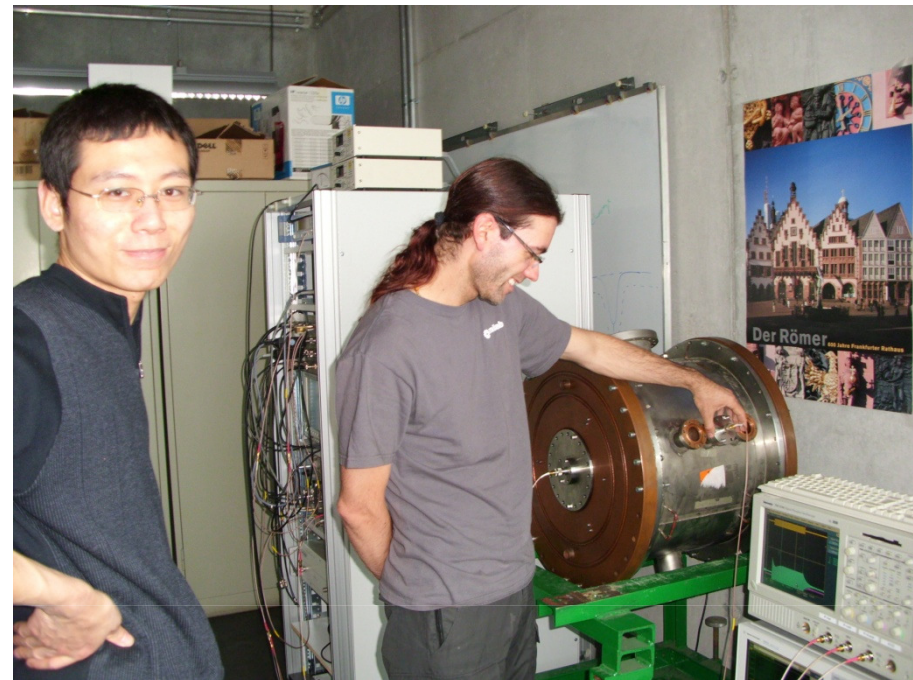
$$W(t) \sim E(t)^2 \Rightarrow \tau = 2 \tau_L$$

τ_L : decay time of the stored energy in the cavity

$$\Rightarrow Q_L = \omega \cdot \tau_L \quad : \text{loaded quality factor}$$

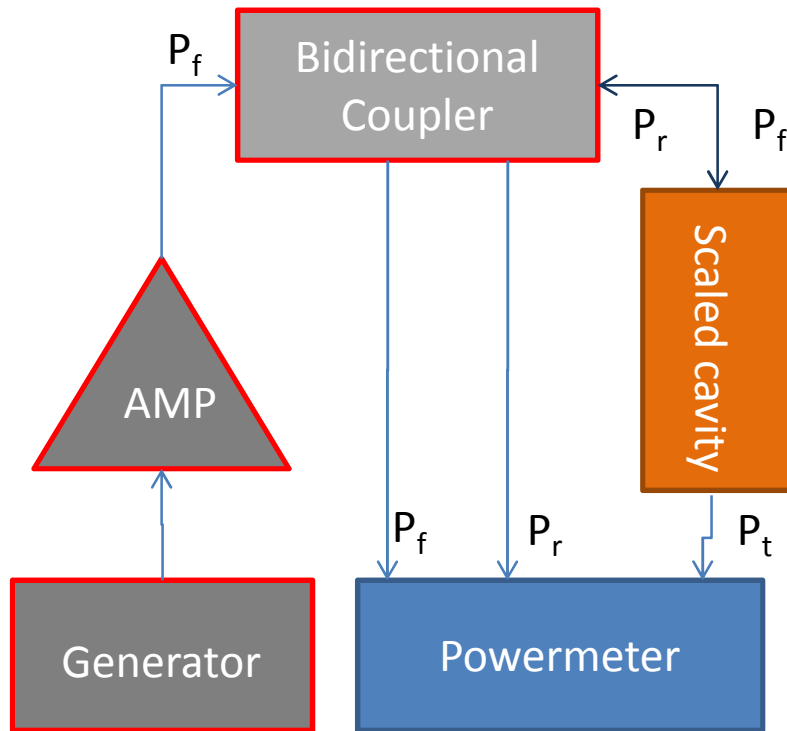
$$\Rightarrow Q_0 = Q_L \cdot (1 + \beta) \quad : \text{intrinsic quality factor}$$

$$\Rightarrow P_r^{\text{on}} = P_r^{\text{off}} \Leftrightarrow \beta = 1 \quad (\text{critical coupling}) \Rightarrow Q_0 = 2Q_L$$



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Perturbation Capacitor method
=> shunt impedance

$$f_{per} = \frac{1}{2\pi\sqrt{L(C+\Delta C)}} \Leftrightarrow C = \frac{\Delta C}{(f/f_{per})^2 - 1}$$

$$R_p = \frac{U^2}{P} = \frac{2Q_0}{\omega C}$$

Measurements at scaled Model

		Analytical	MWS	Measured (Powermeter)
Effective Inductance	μH	12.9	12.3	12.5
Effective Capacitance	pF	23.8	31.1	28.8
Frequency	MHz	9.09	8.26	8.37
Intrinsic Quality Factor		2986	3058	1772
Shunt impedance	$\text{M}\Omega$	4.4	3.9	2.8

- Good agreement for the Inductance
- Stray Capacitance underestimated => higher frequency
- ~ 60% of the calculated intrinsic quality factor can be reached
- Measurements with network analyzer give comparable results
- Analytic formulas are good enough for “first shot” estimations
- big loops ($\sim 120 \times 62 \text{mm}^2$) are needed for critical coupling
=> mechanical problems + RF-properties of the loop
- alternative coupling methods (capacitive, galvanic) have to be investigated

Outlines:

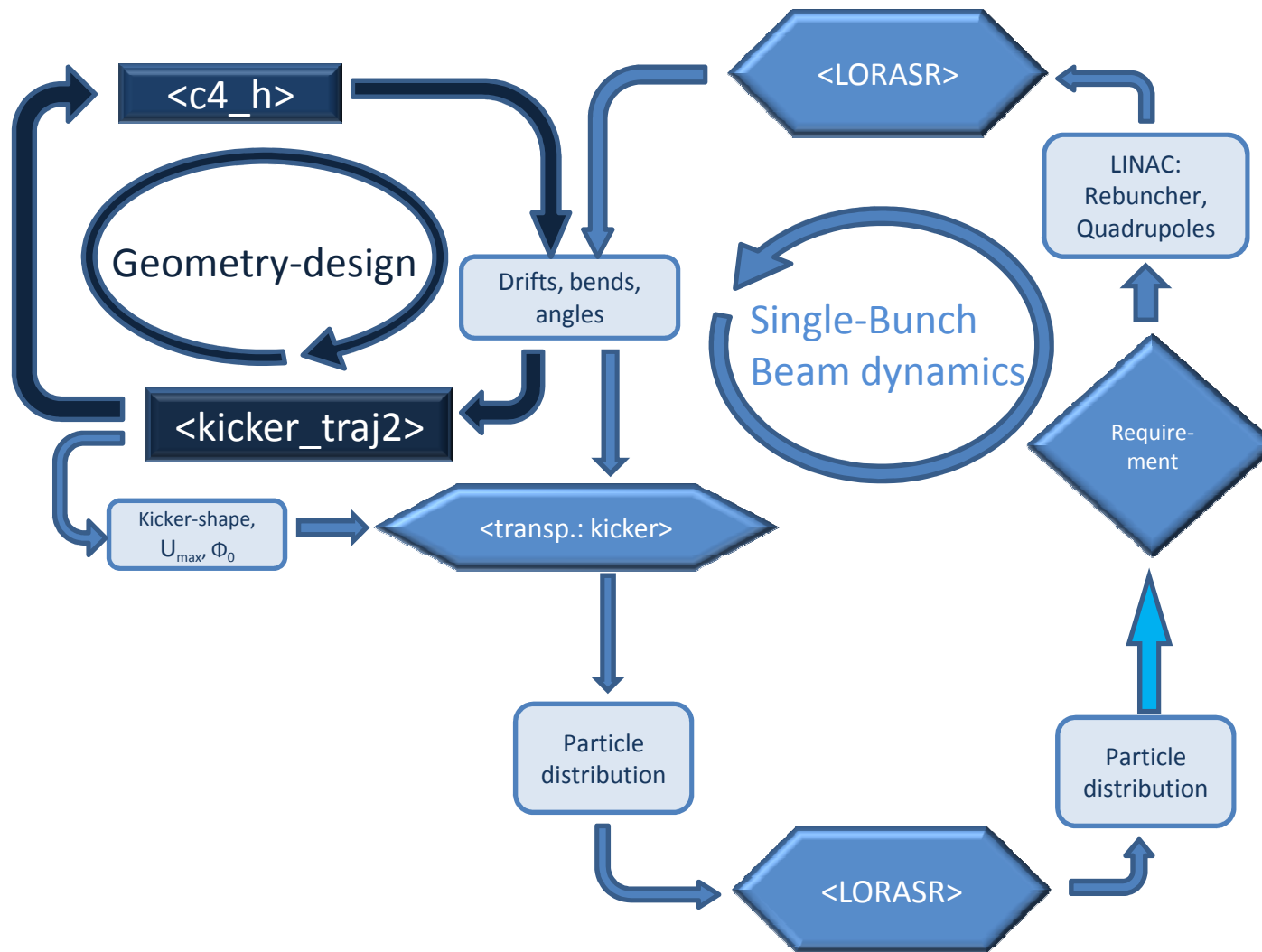
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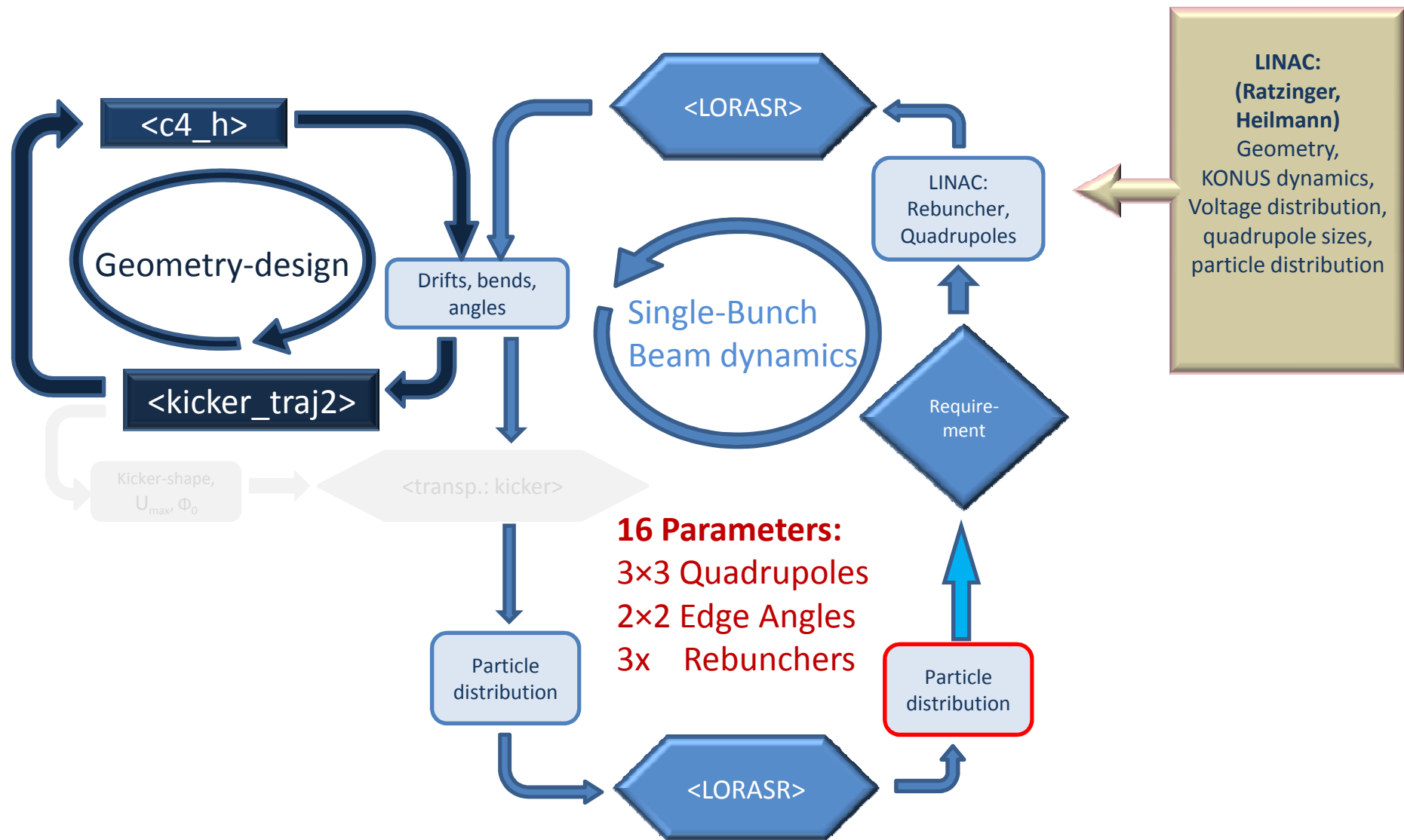
- Outlook

Bunch Compressor: Design / Optimization Cycles

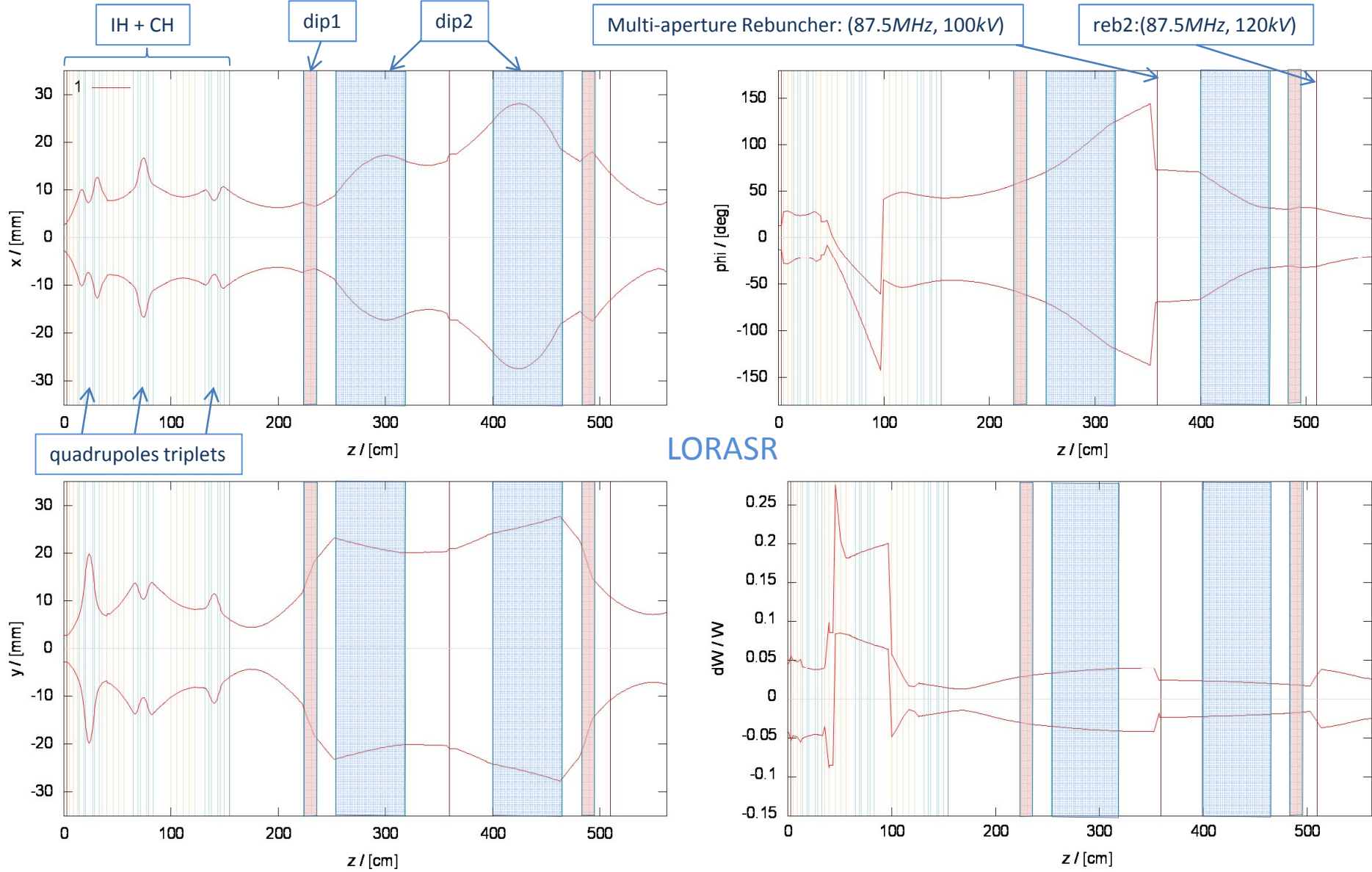


LINAC:
(Ratzinger, Heilmann)
 Geometry,
 KONUS dynamics,
 Voltage distribution,
 quadrupole sizes,
 particle distribution

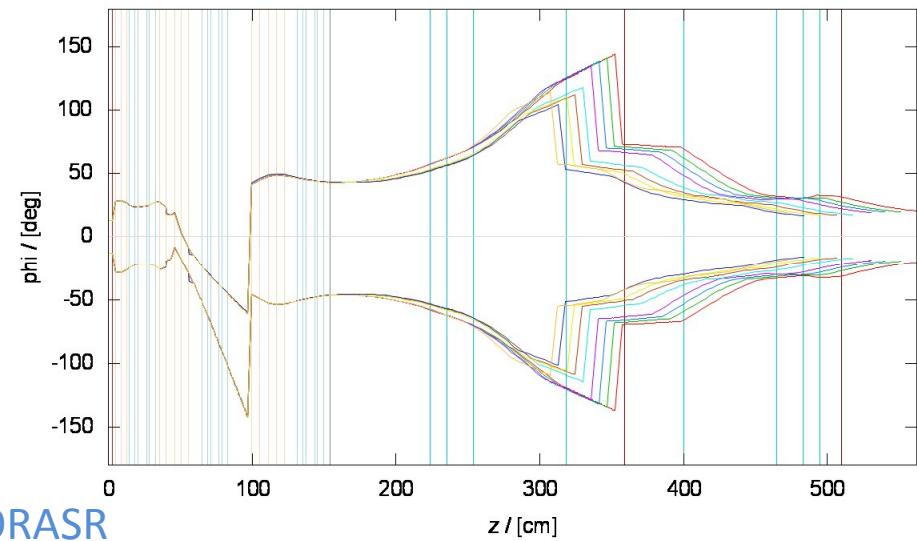
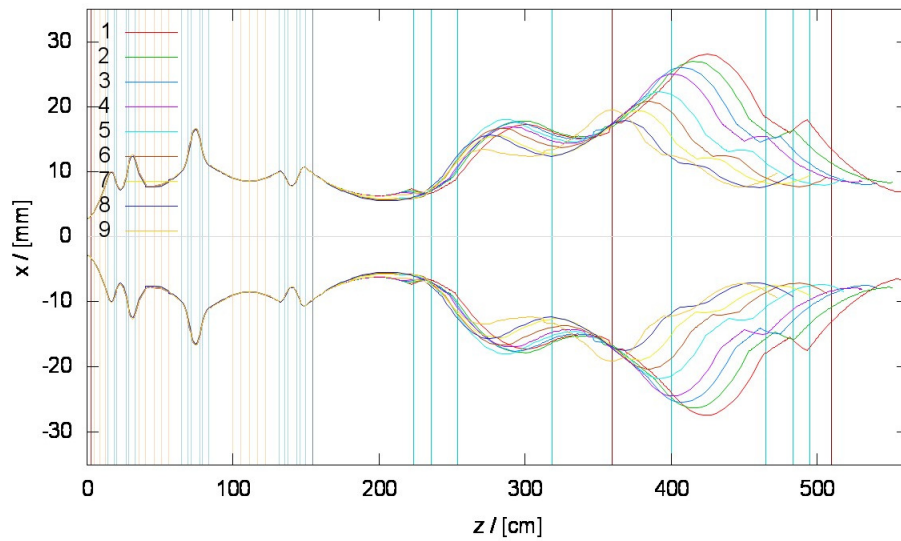
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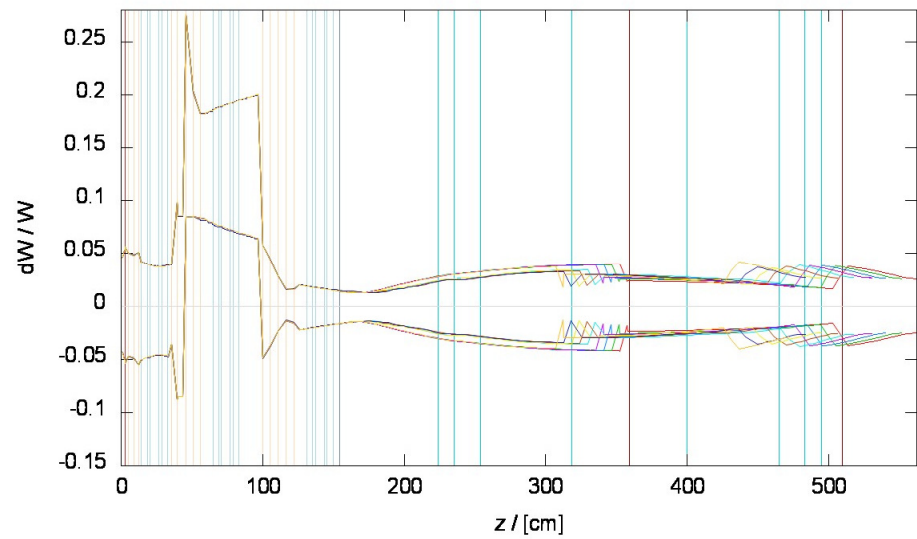
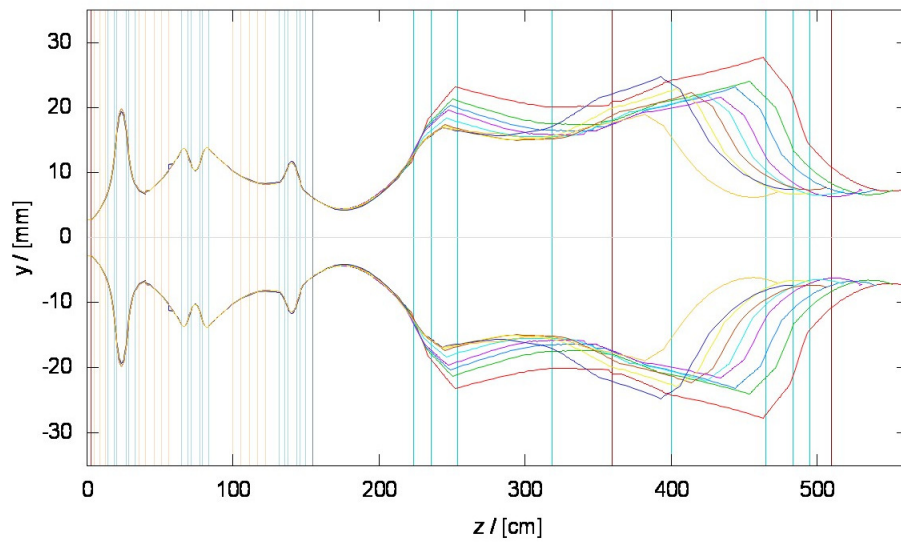
Bunch Compressor: Envelopes(95%) – bunch(1)



Bunch Compressor: Envelopes(95%) – bunch(all)

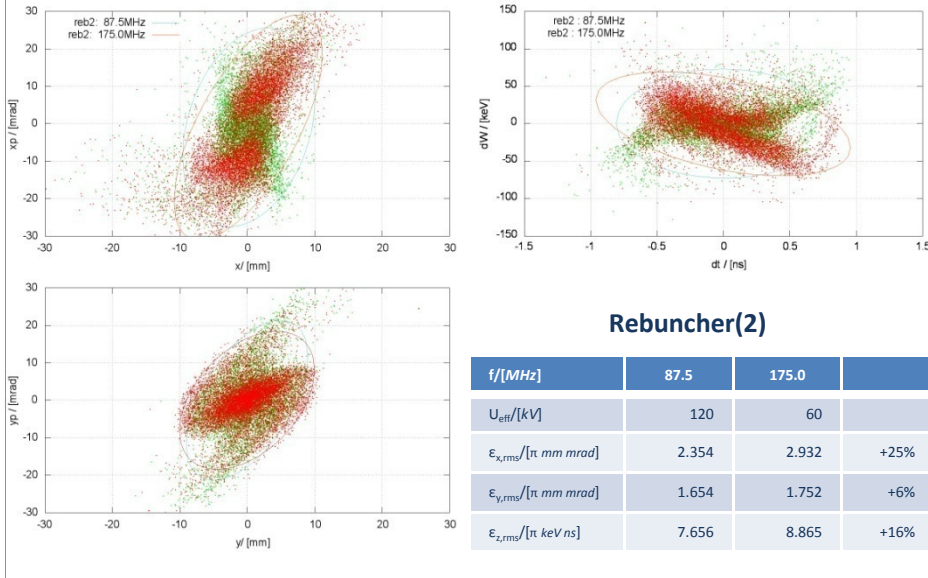


LORASR

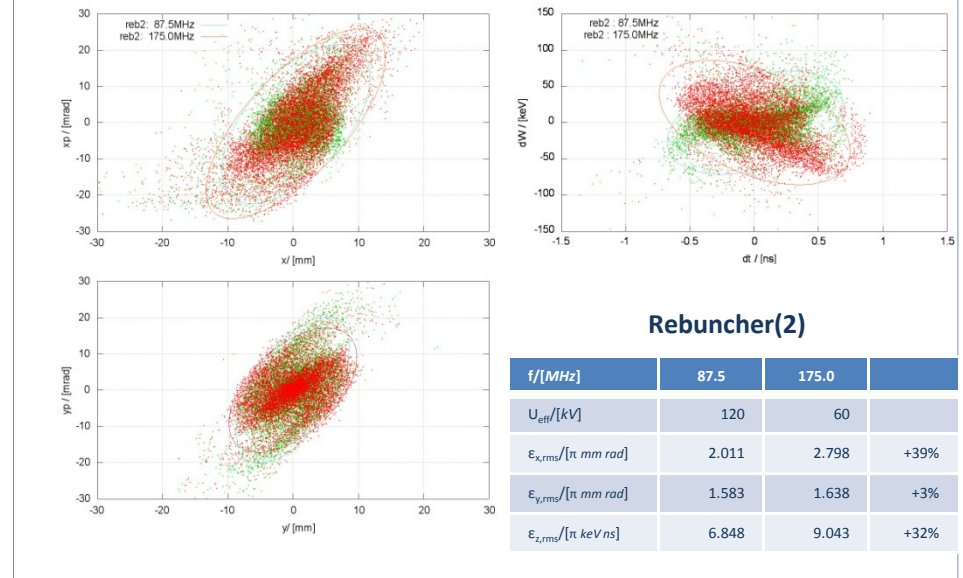


Bunch Compressor: projections at the target

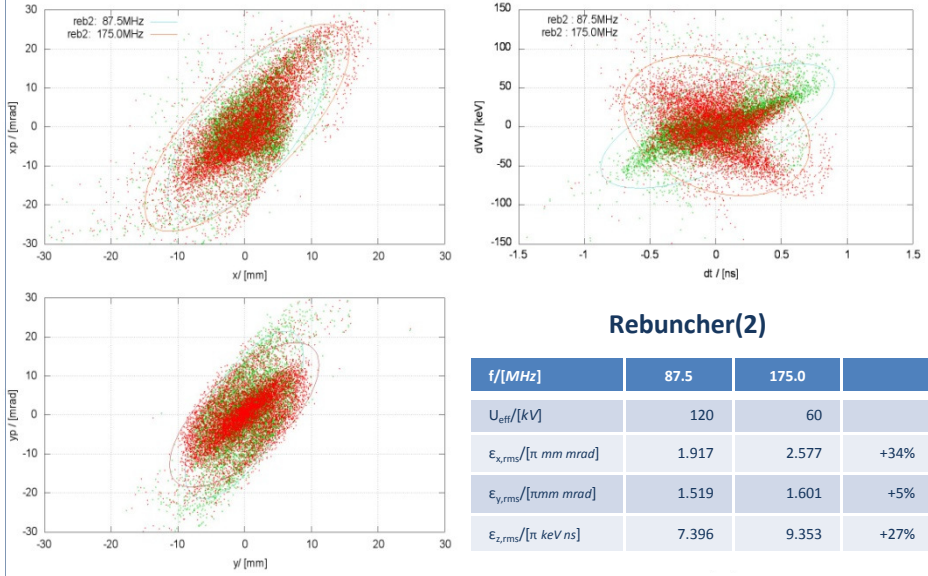
Bunch(1)



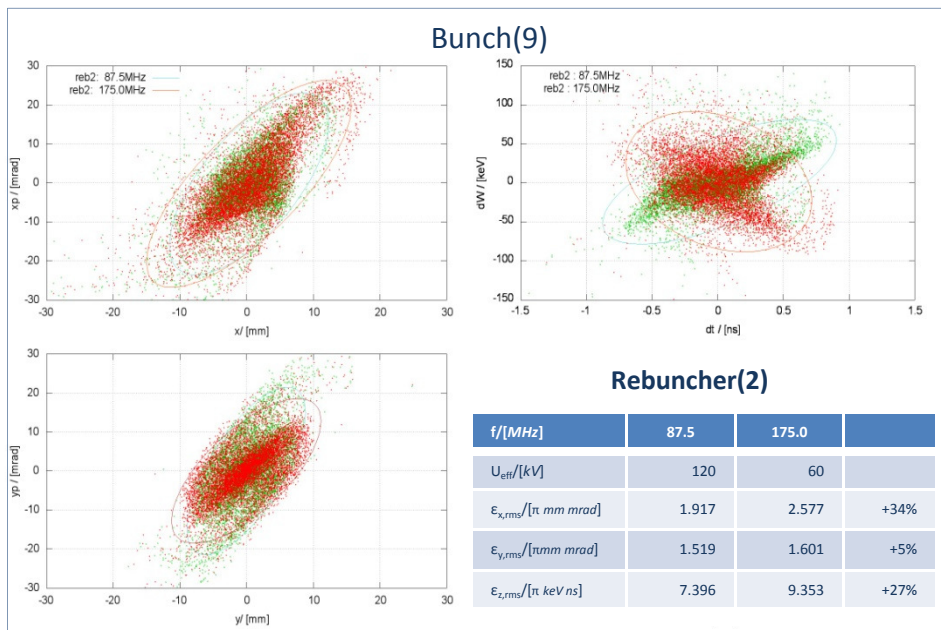
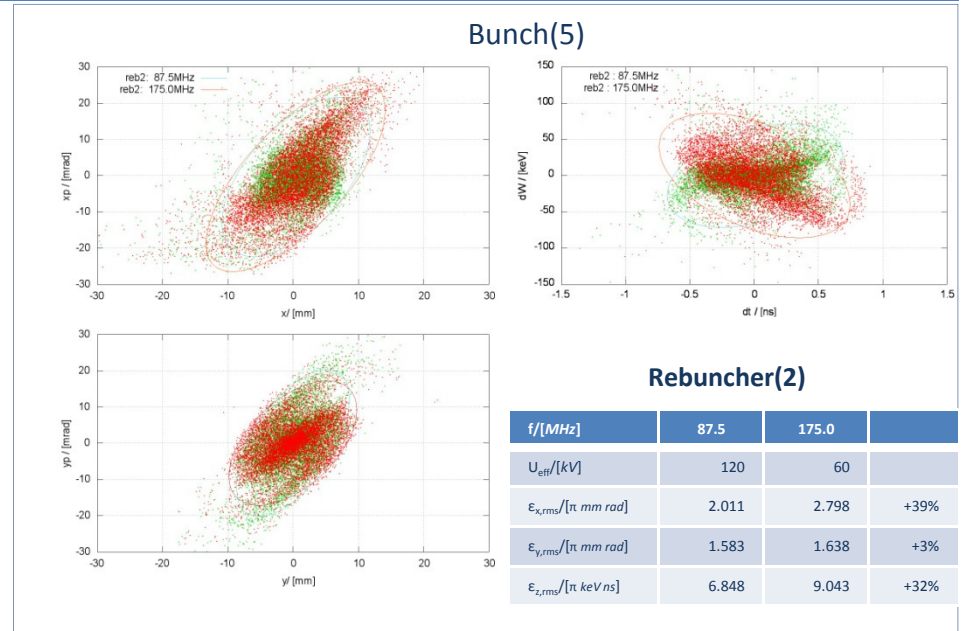
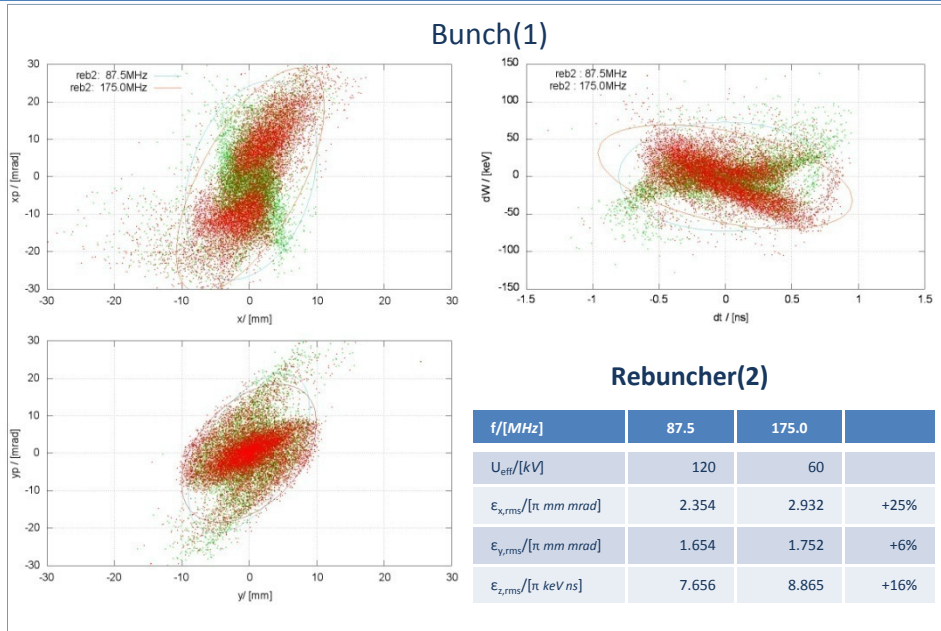
Bunch(5)



Bunch(9)



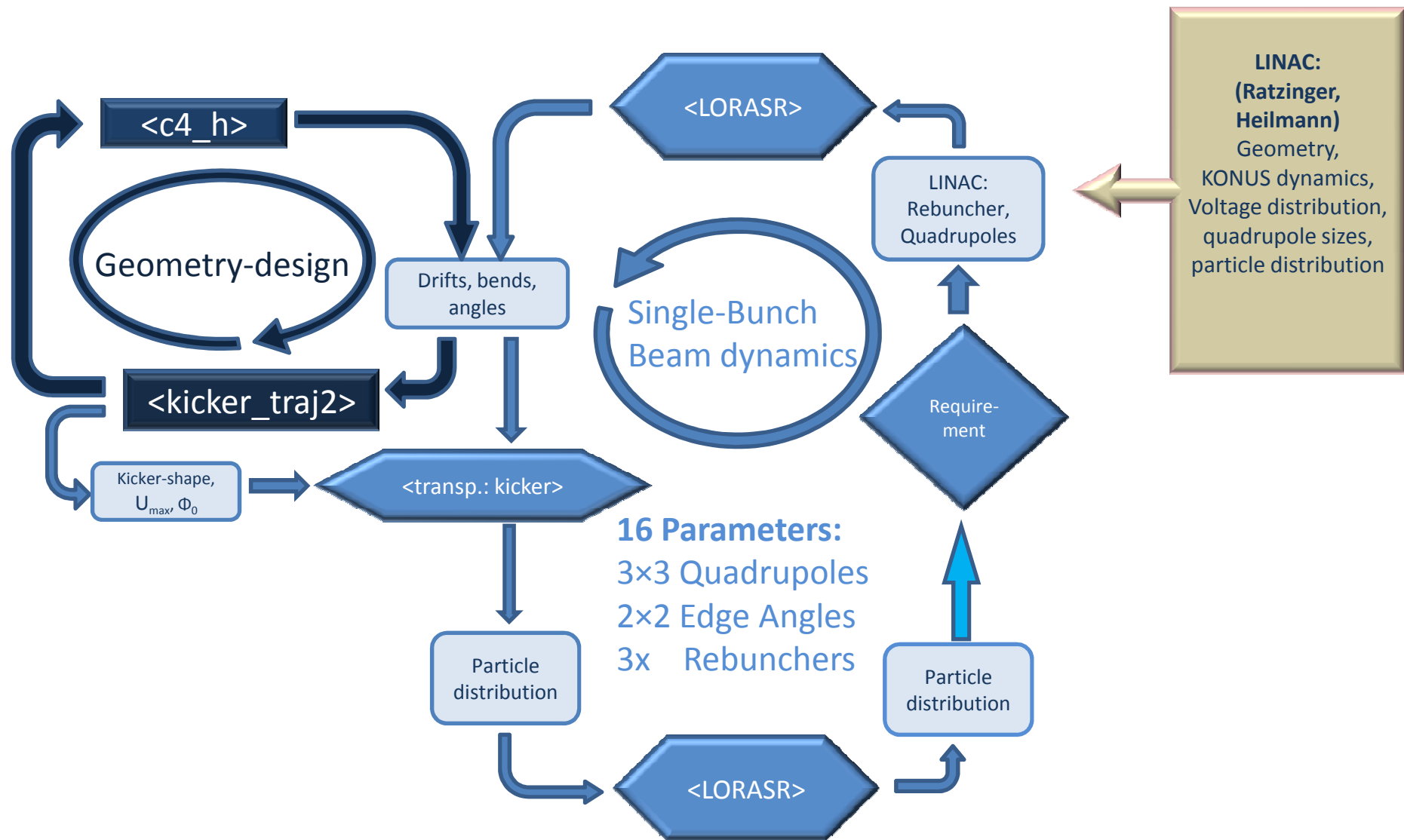
Bunch Compressor: projections at the target



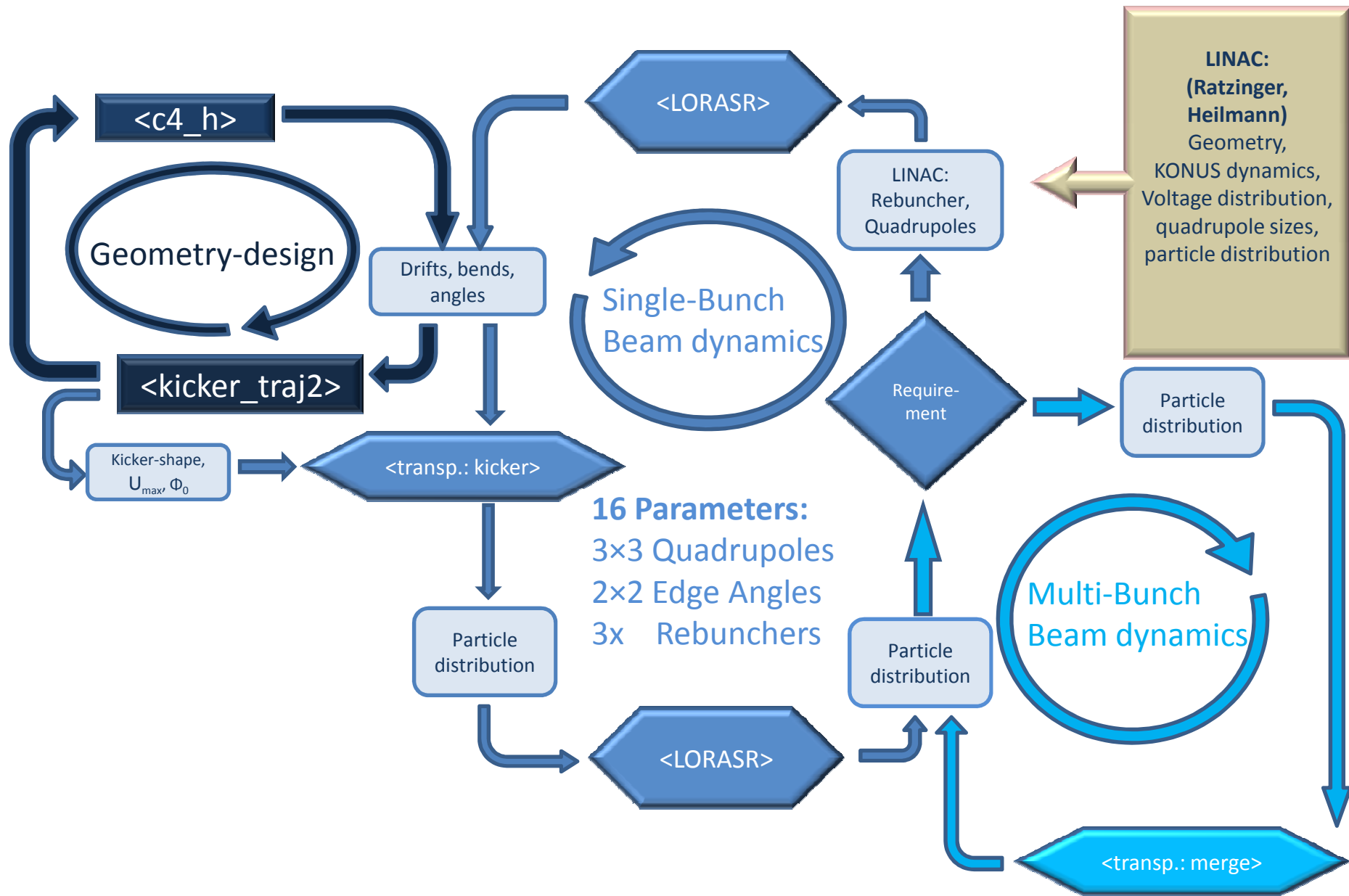
Single Bunch Beam Dynamics:

- ✓ • $N_{\text{bunch}} = 9$
- ✓ • $\Delta T = 50\text{-}100\text{ ns} \Rightarrow \Delta T \approx 1\text{ ns}$
- ✓ • $A_{(\text{beam at target})} < 3 \times 3 \text{ cm}^2$
- ✓ • $I_{(\text{per pulse})} \approx 8\text{ A}$
- ✓ • $\Delta W < \pm 5\%$

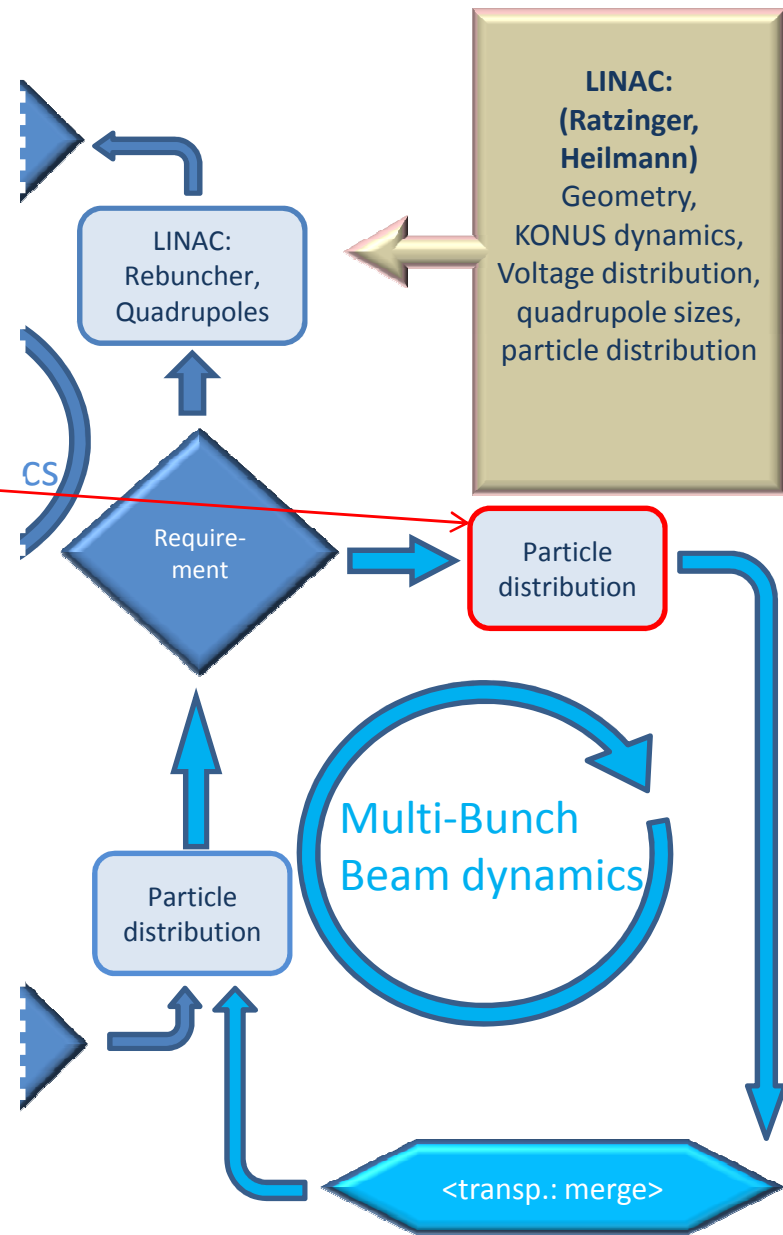
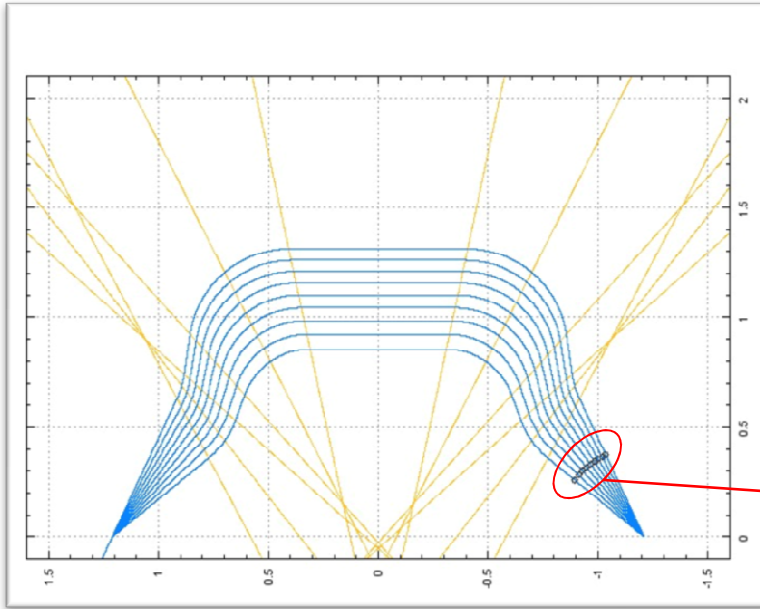
Bunch Compressor: Design / Optimization Cycles



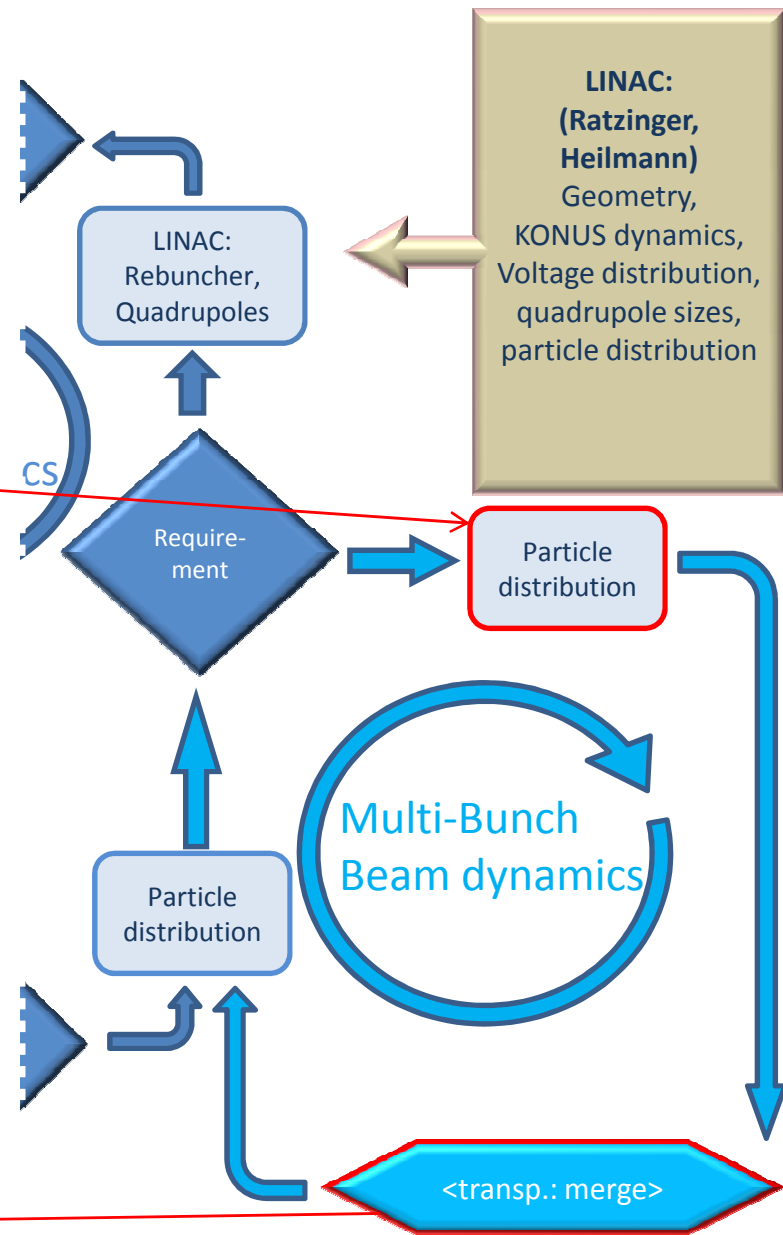
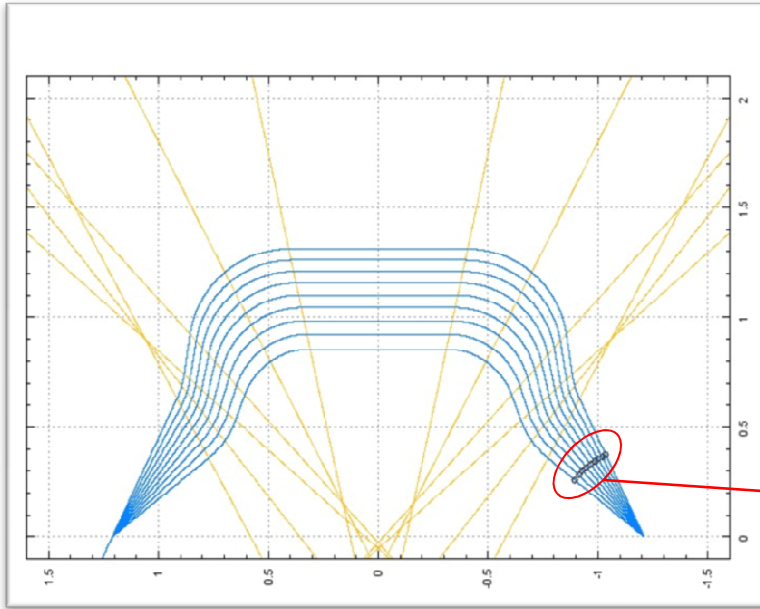
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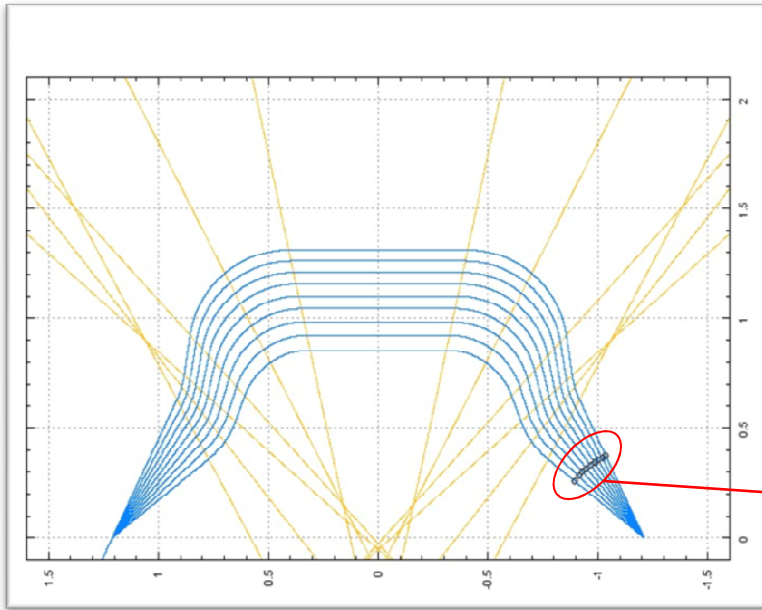


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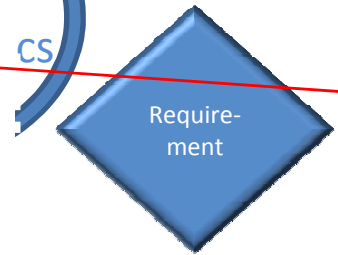
- <transp.:merge>:**
- Particle in Cell (PIC)
 - dynamic lattice
 - finite differences
 - Poisson solver

Bunch Compressor: Design / Optimization Cycles

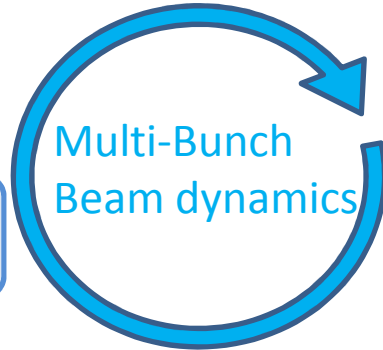


**LINAC:
(Ratzinger,
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Geometry,
KONUS dynamics,
Voltage distribution,
quadrupole sizes,
particle distribution

LINAC:
Rebuncher,
Quadrupoles



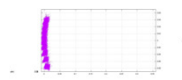
Particle
distribution

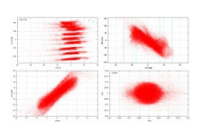


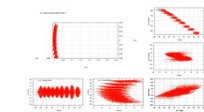
Particle
distribution

<transp.: merge>

L	= 35cm
I	= 9x150mA
N _{particle}	≈ 90k
N _{grid}	= 100x100x100
Δ x _{stepsize}	= 1mm
Δ t _{calc+plot}	≈ 50s

merge 

Projections at target 

projections 

<transp.:merge>

- Particle in Cell (PIC)
- dynamic lattice
- finite differences
- Poisson solver

Outlines:

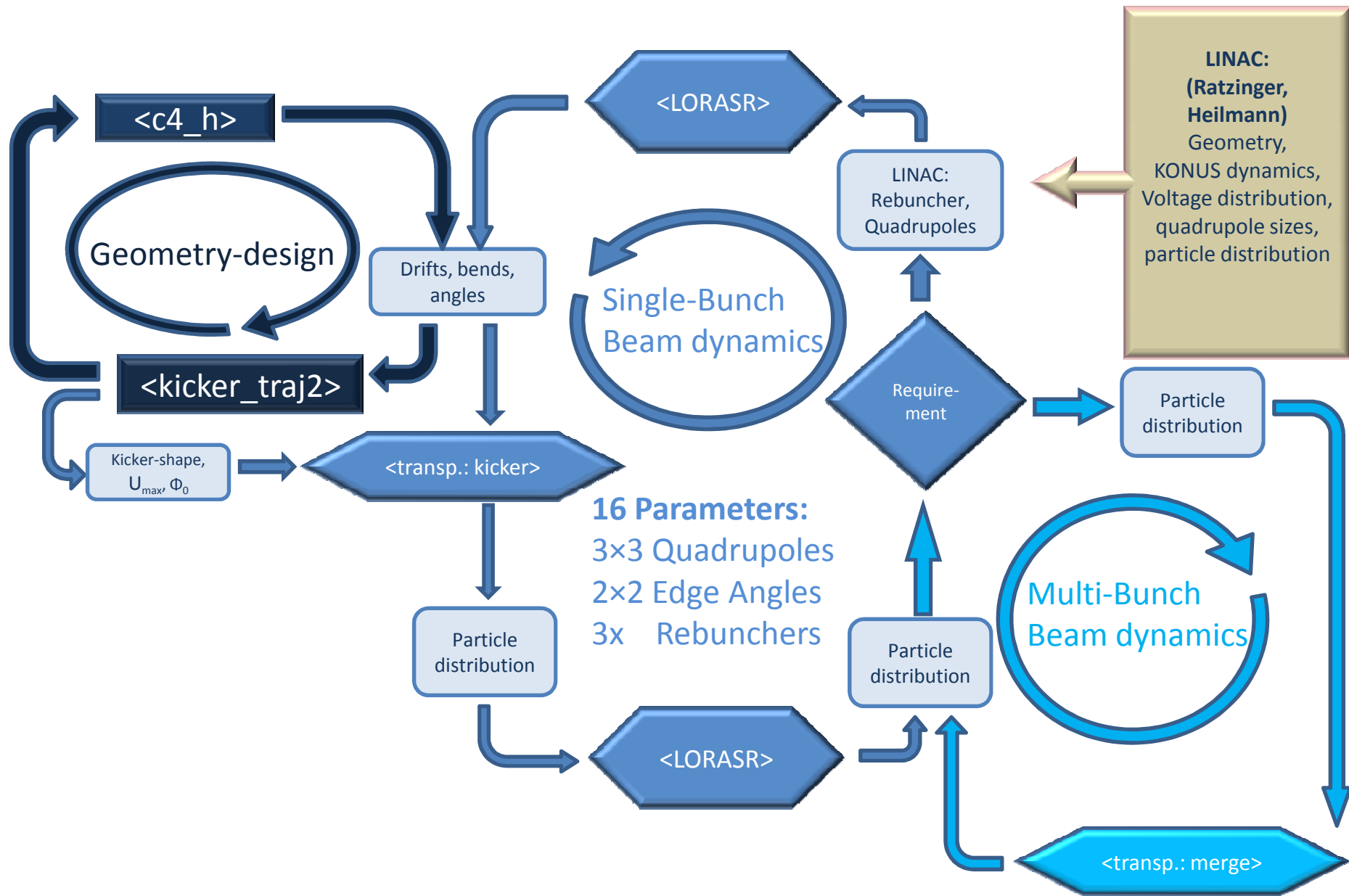
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○ **Design / Optimization Cycles**

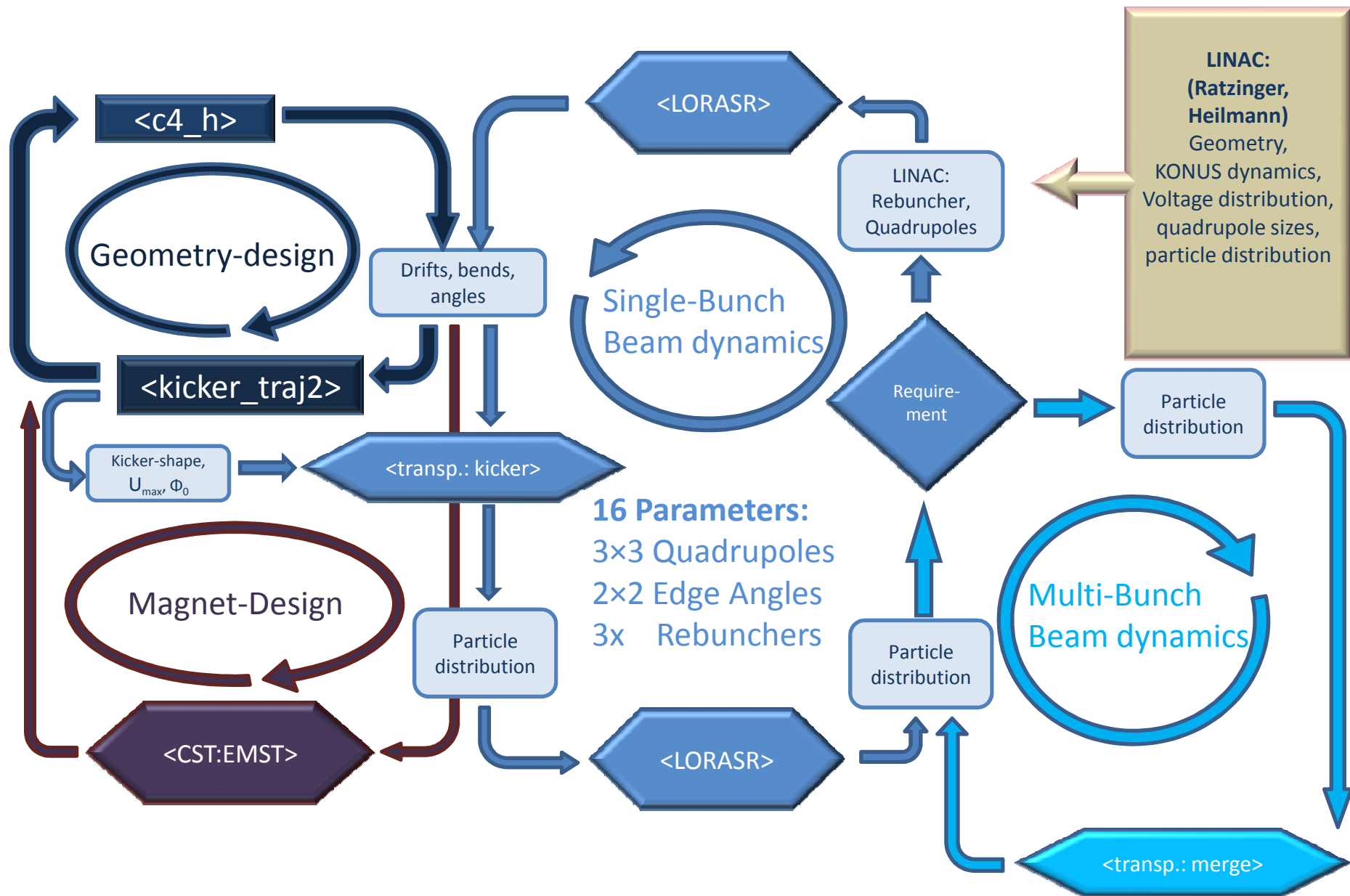
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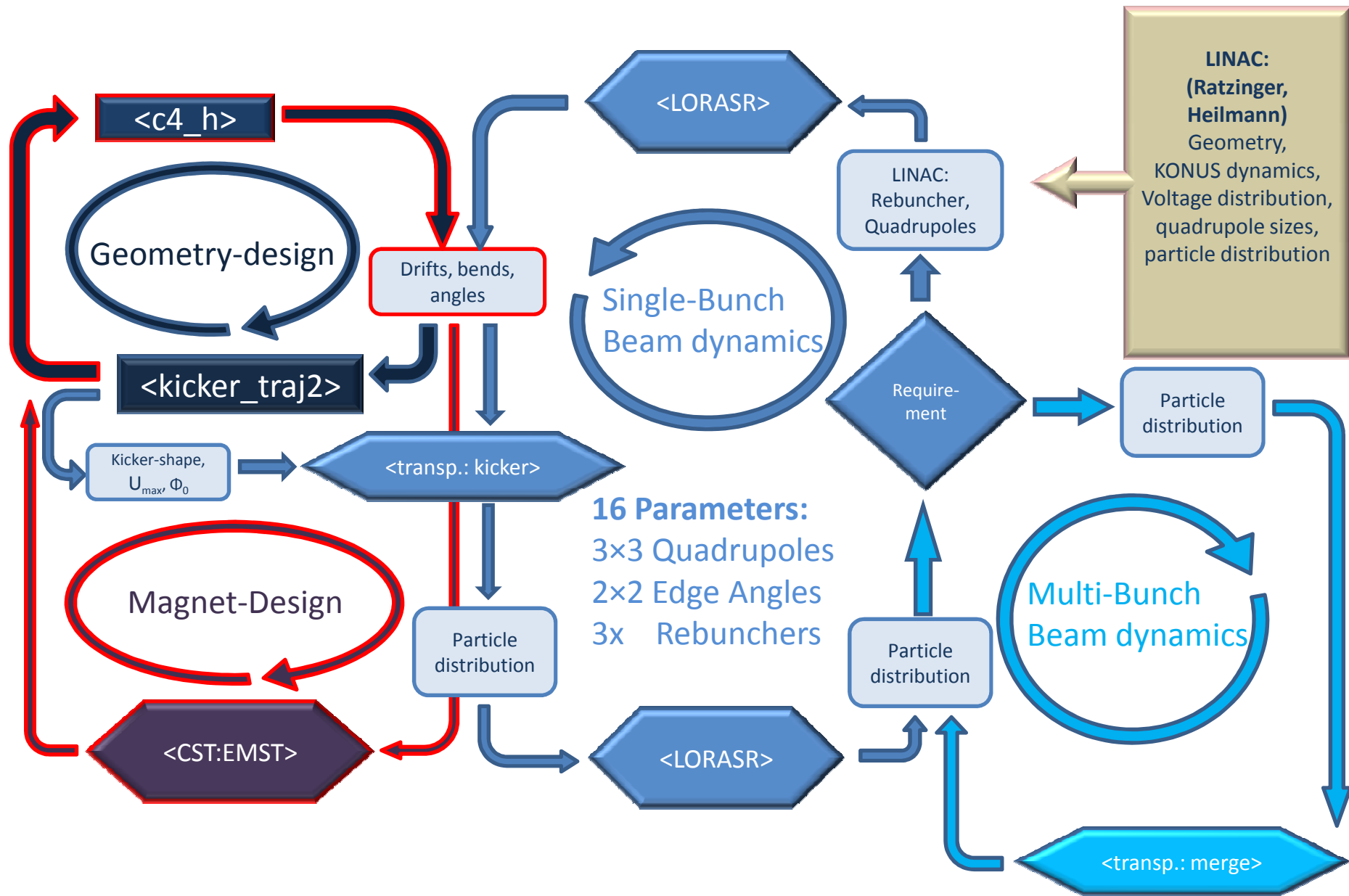
Bunch Compressor: Design / Optimization Cycles



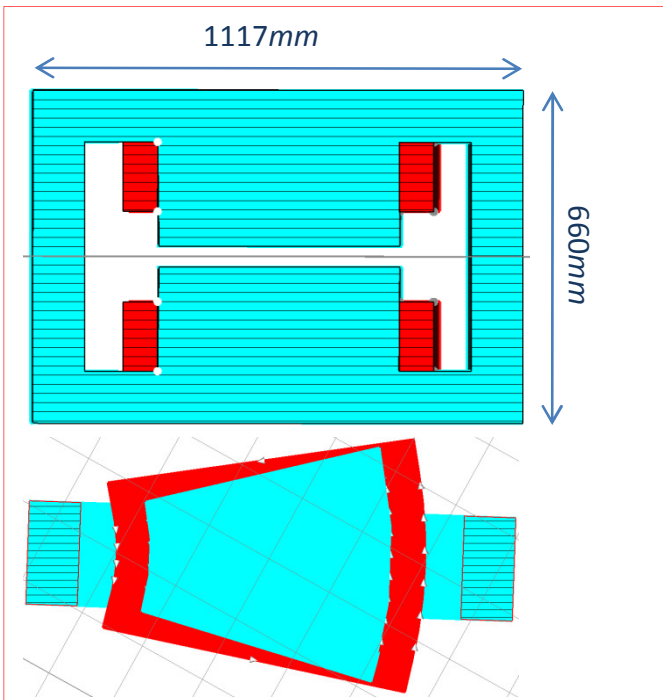
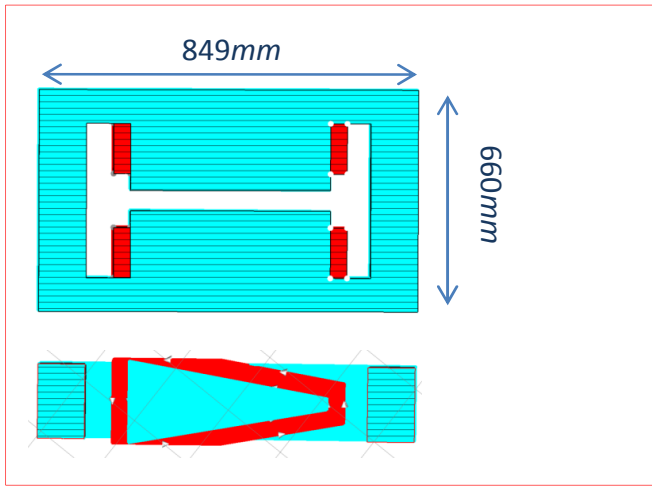
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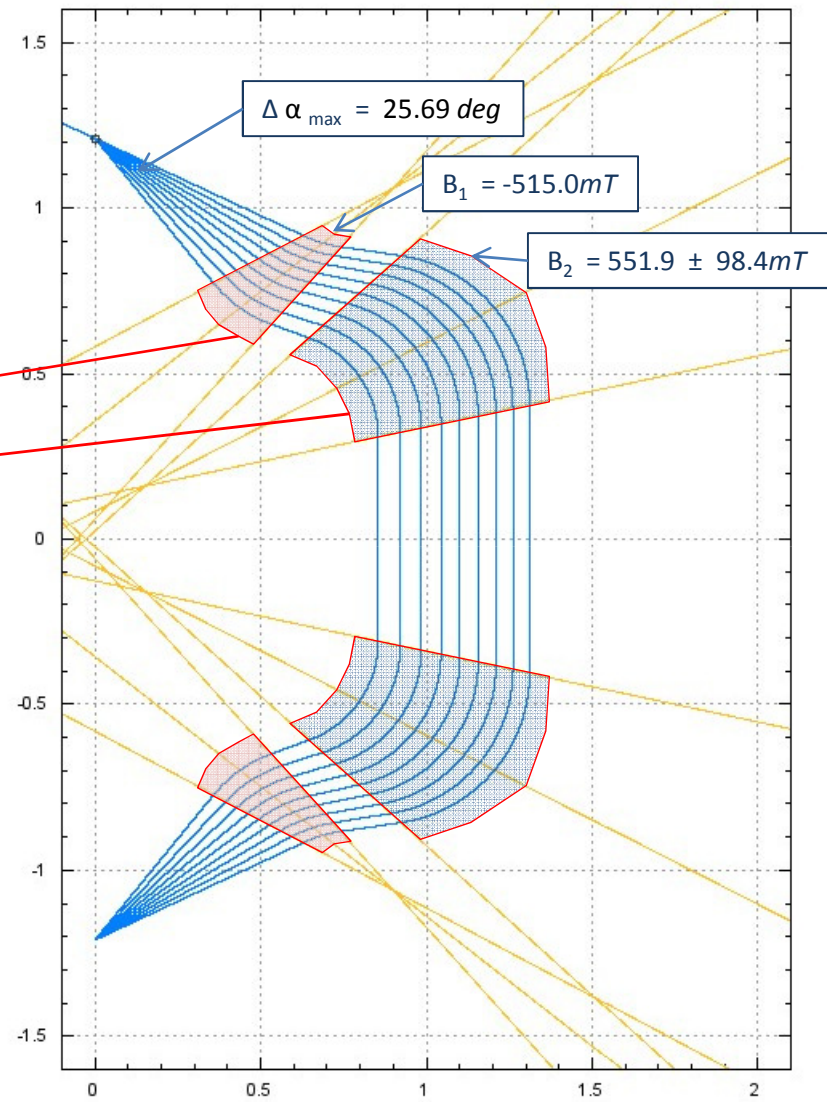
Bunch Compressor: Design / Optimization Cycles



Bunch Compressor: Dipoles

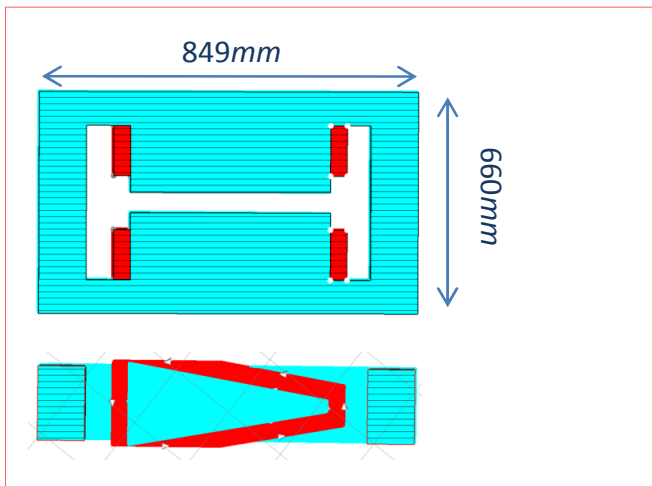


Geometry: g9_5x

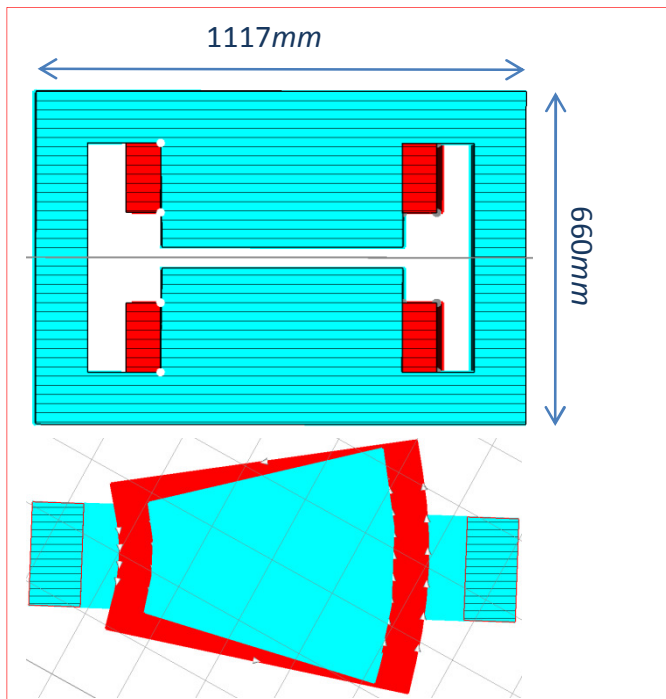
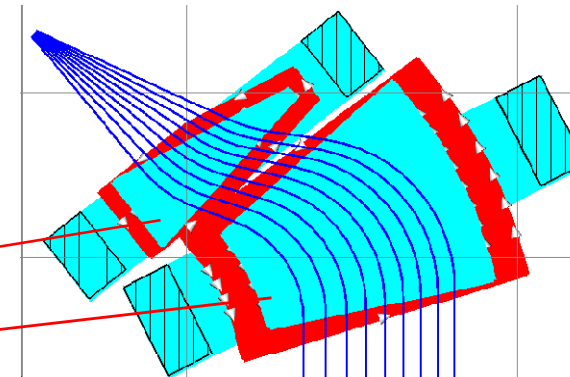


Bunch Compressor: Dipoles

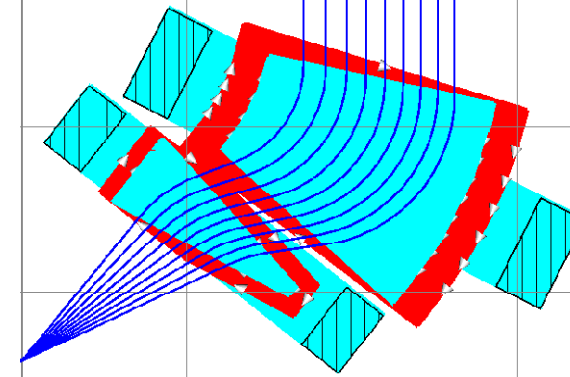
Geometry: g9_5x



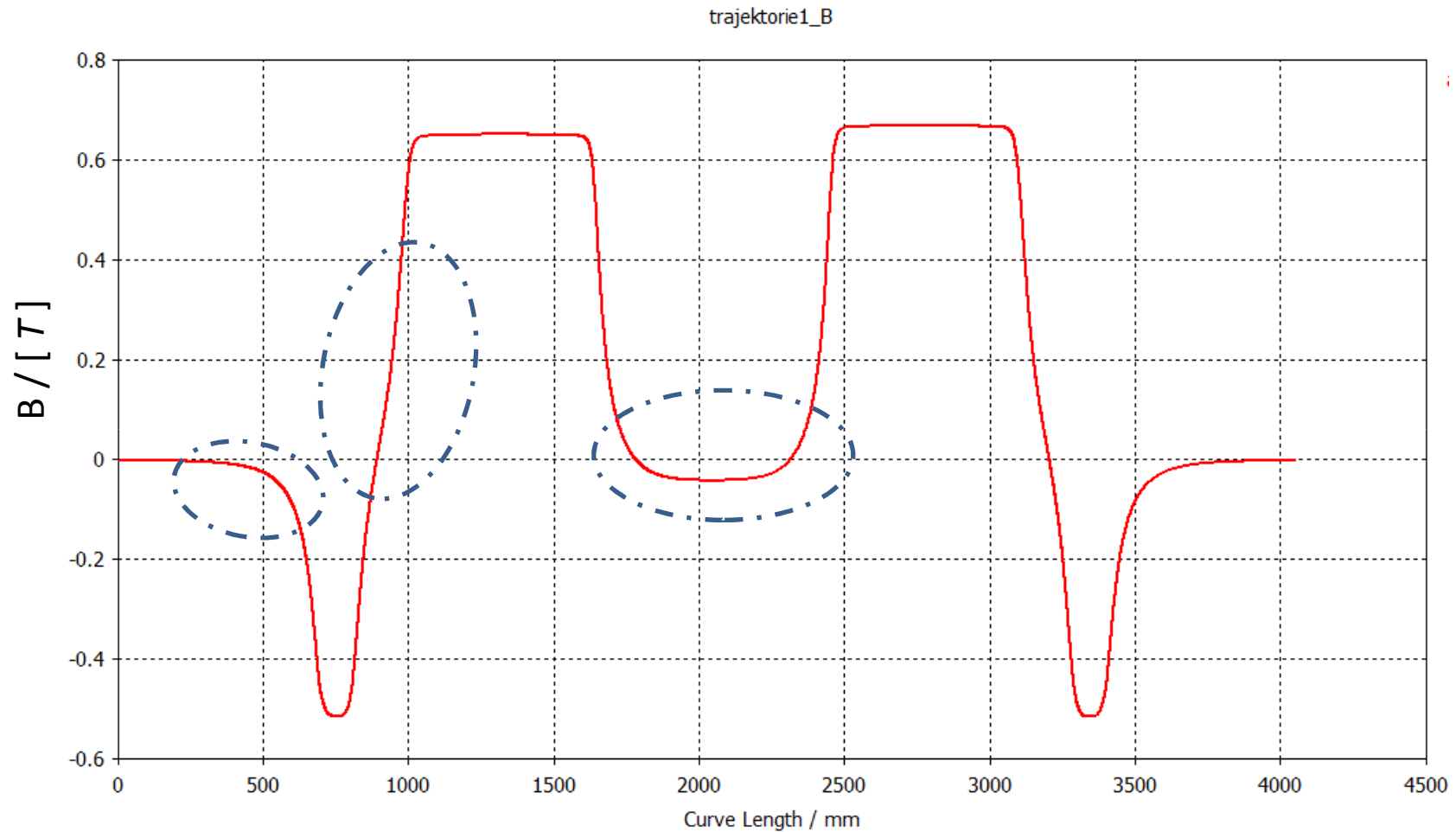
Dipole(1)	
B_1 /[mT]	515
g /[mm]	60
$N \cdot I$ /[A]	10420
A_{coil} /[mm ²]	50×150
A_{wind} /[mm ²]	7×7
N	153
I /[A]	68



Dipole(2)	
B_2 /[mT]	650
g /[mm]	60
$N \cdot I$ /[A]	60476
A_{coil} /[mm ²]	100×200
A_{wind} /[mm ²]	7×7
N	408
I /[A]	148



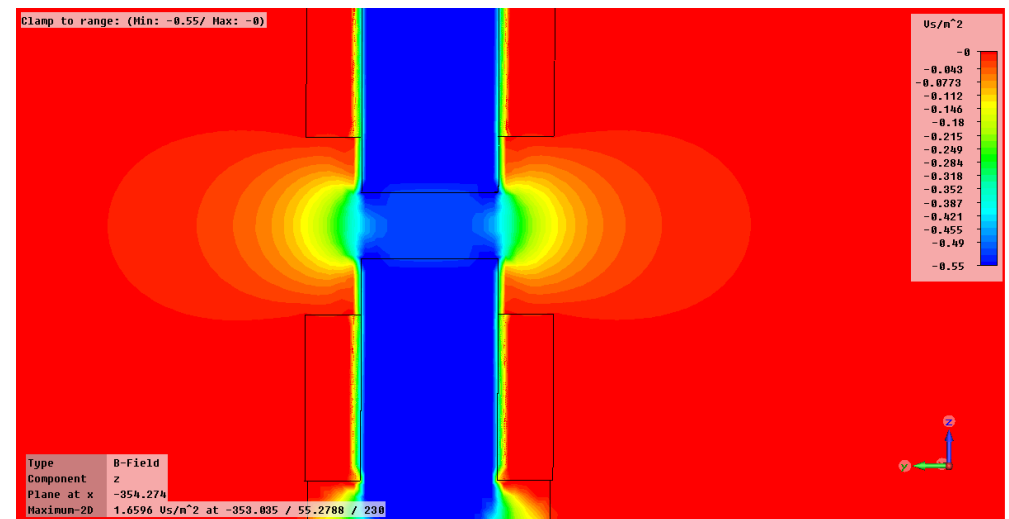
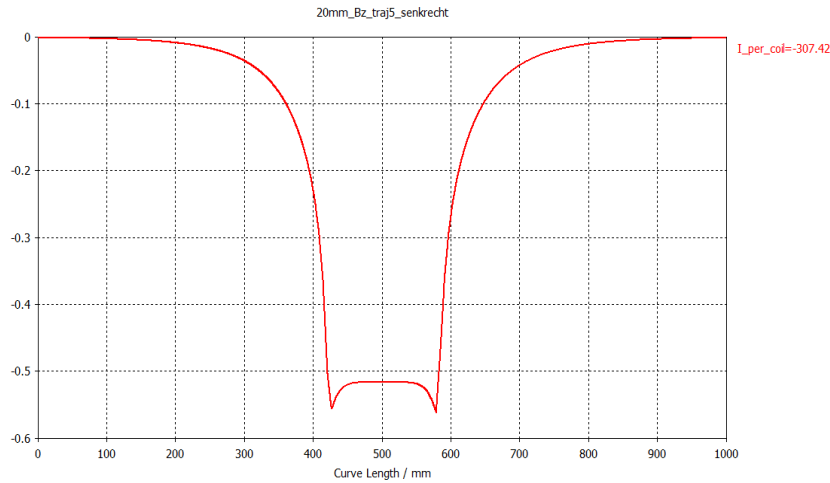
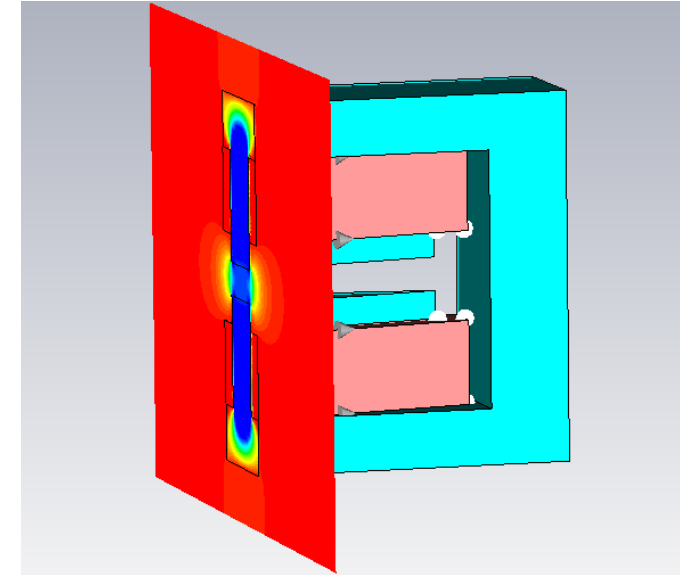
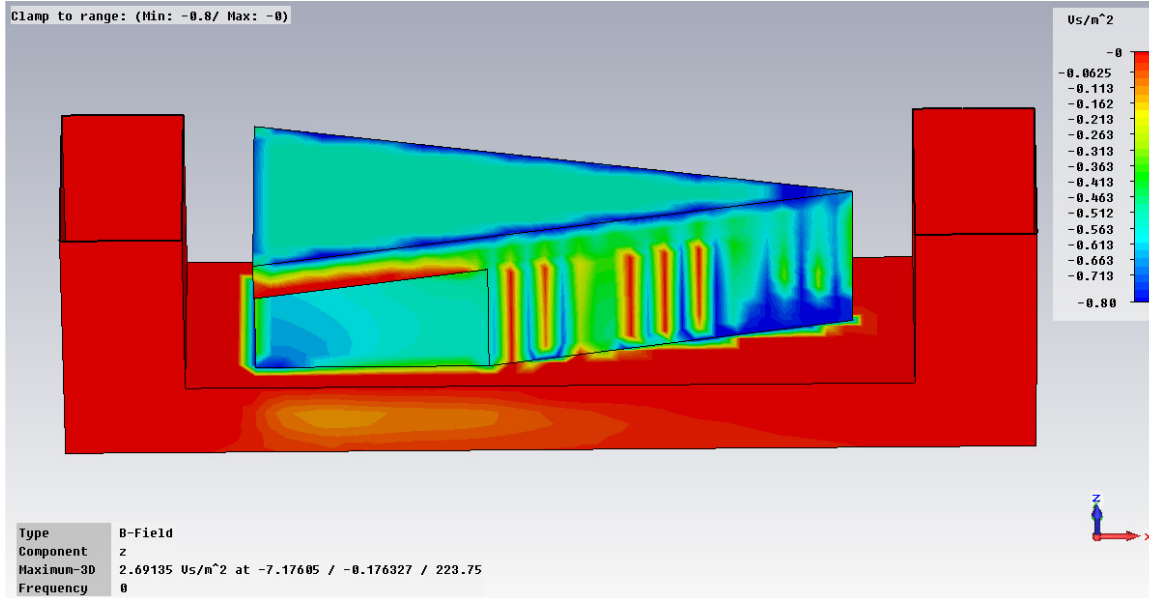
Bunch Compressor: field along the first trajectory at preliminary dipole design



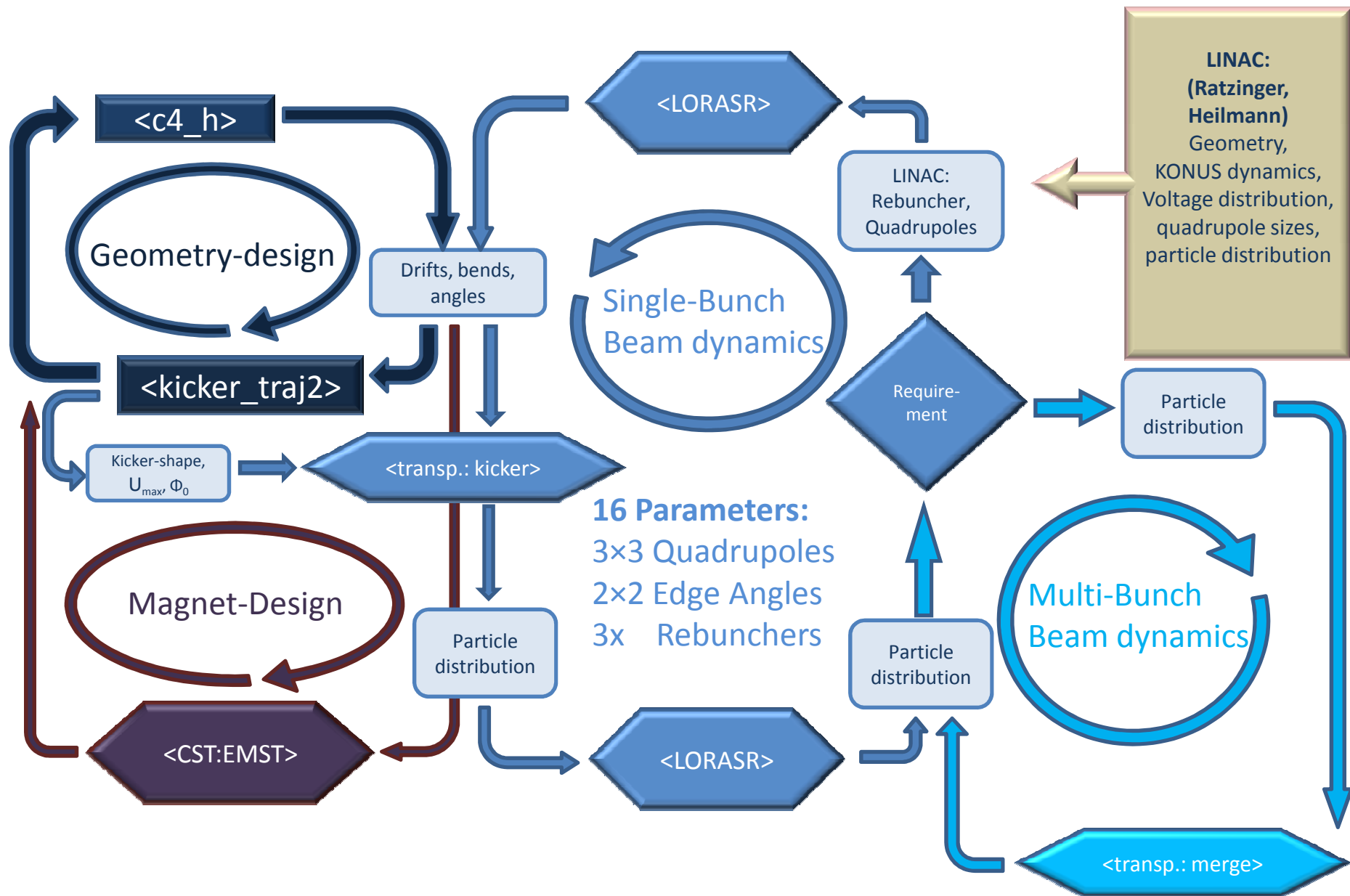
- large fringing field
- Connected fringing field region

=> Effects of fringing fields on beam dynamics?

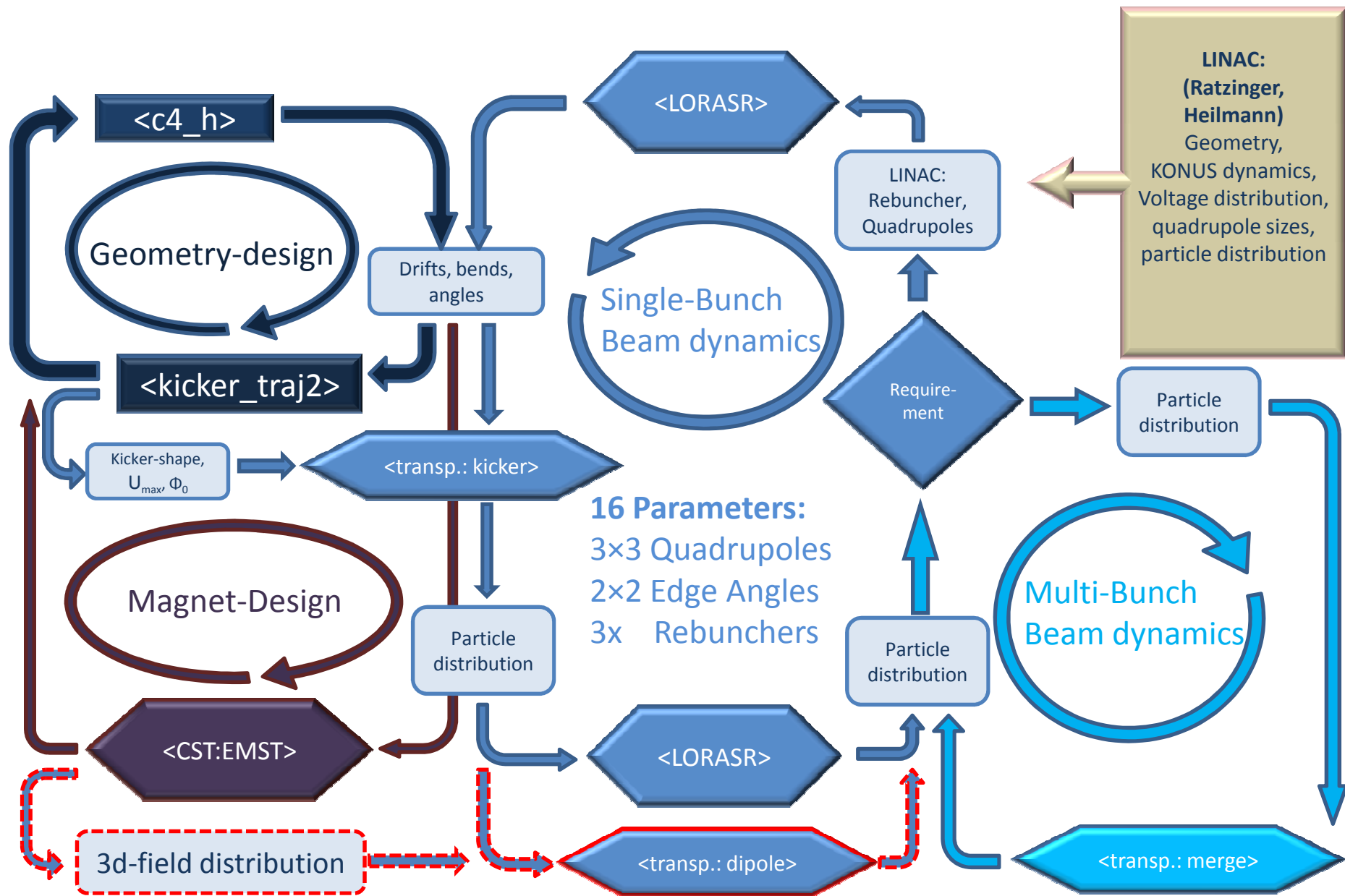
field enhancement at the edges due to saturation effects



Bunch Compressor: Design / Optimization Cycles



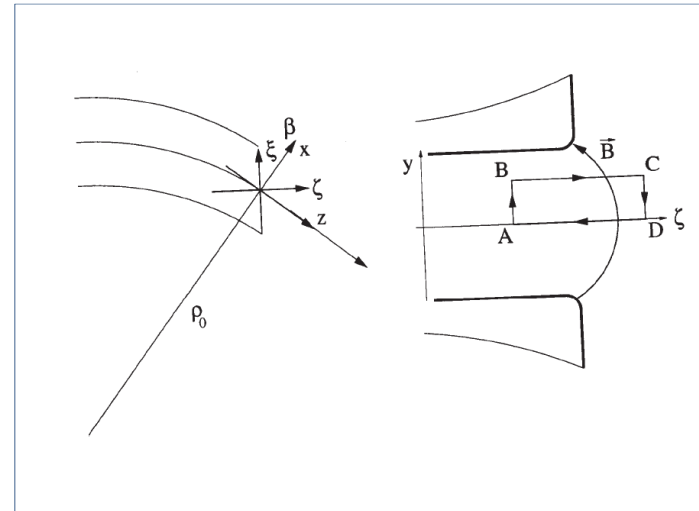
Bunch Compressor: Design / Optimization Cycles



The complete effect of the fringing field is applied in one instantaneous kick in the transverse planes:

$$x' = x'_0 + k_x(\phi, \rho_0) \cdot x_0 \quad \rightarrow \Delta x'$$

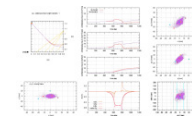
$$y' = y'_0 + k_y\left(\phi, \frac{g}{\rho_0}, K\right) \cdot y_0 \quad \leftarrow \Delta y'$$



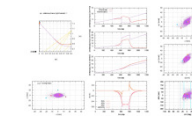
Parameters of the first dipole:

Fringing field Integral \underline{K}	=	1.034
Edge angle ϕ_{entrance}	=	-25.01 [deg]
Edge angle ϕ_{exit}	=	29.31 [deg]
Magnetic field B_0	=	515.0 [mT]
Gap g	=	60.0 [mm]

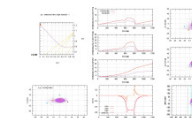
Comparison with realistic field distribution:



0mA: real field dist. vs. matrix



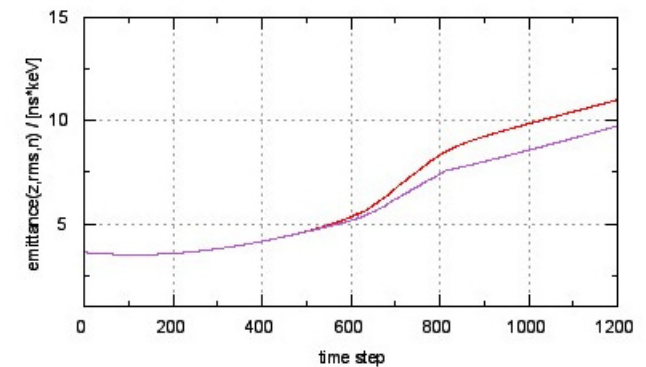
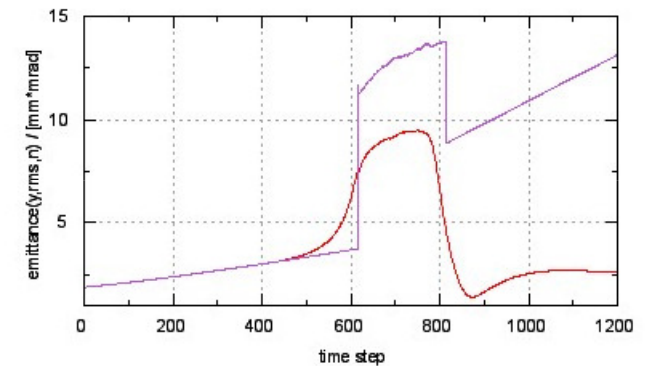
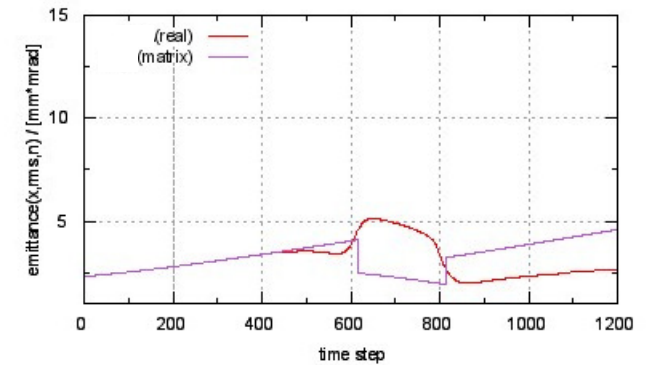
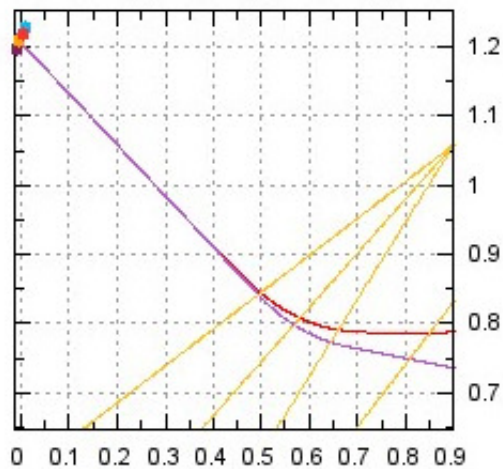
150mA: real field dist. vs. matrix



real field dist.: 0mA vs. 150mA

Beam dynamics with realistic field distribution

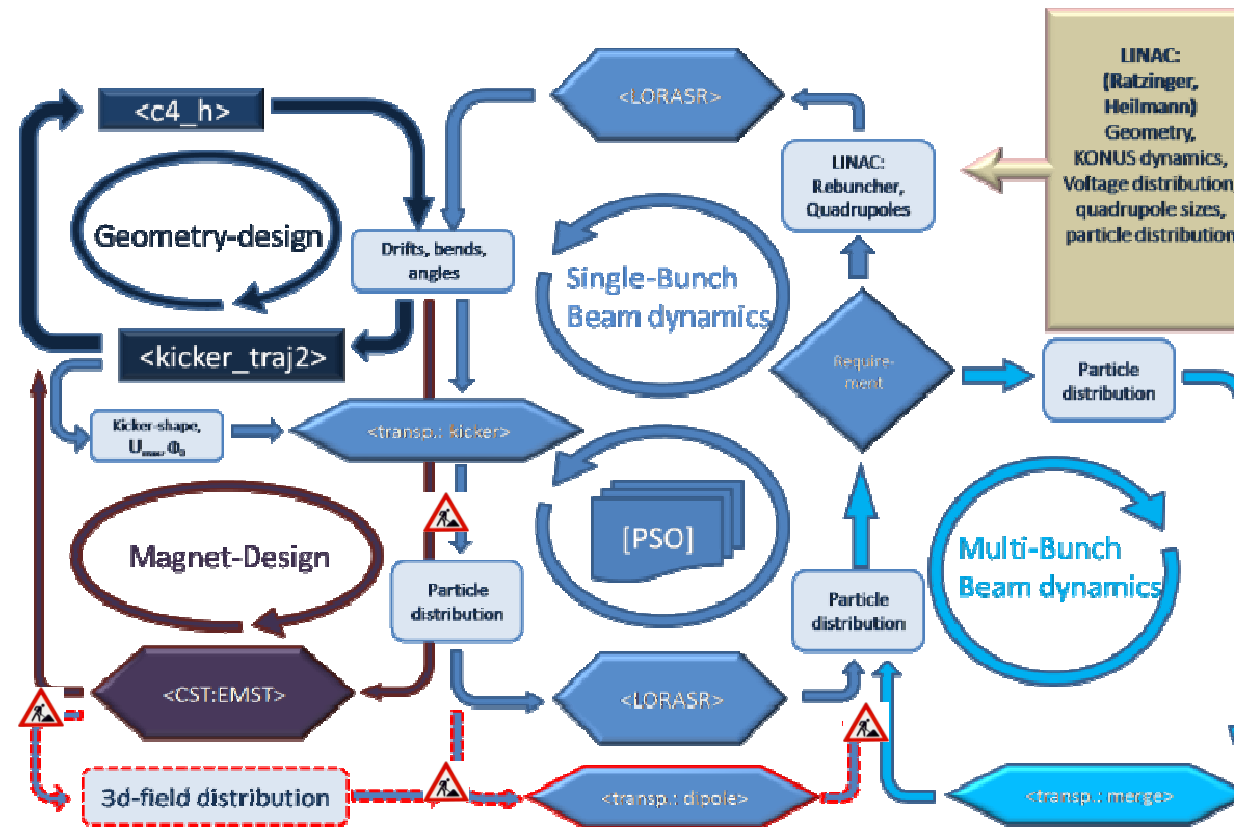
- Center motion significantly changed by large fringing field.
- paraxial approach over estimate the emittance growth in transverse plane.
- bigger emittance growth in long. plane with realistic fields.
- field enhancement nearby the edges due to saturation
Insufficiently described by first order matrix formalism.



Outlines:

- Requirements
- Design / Optimization Cycles
 - Geometry
 - 5MHz Kicker
 - Single Bunch Beam Dynamics
 - Merging Scenario
 - Magnet Design
 - Beam Dynamics with Realistic Field Distributions
- **Outlook**

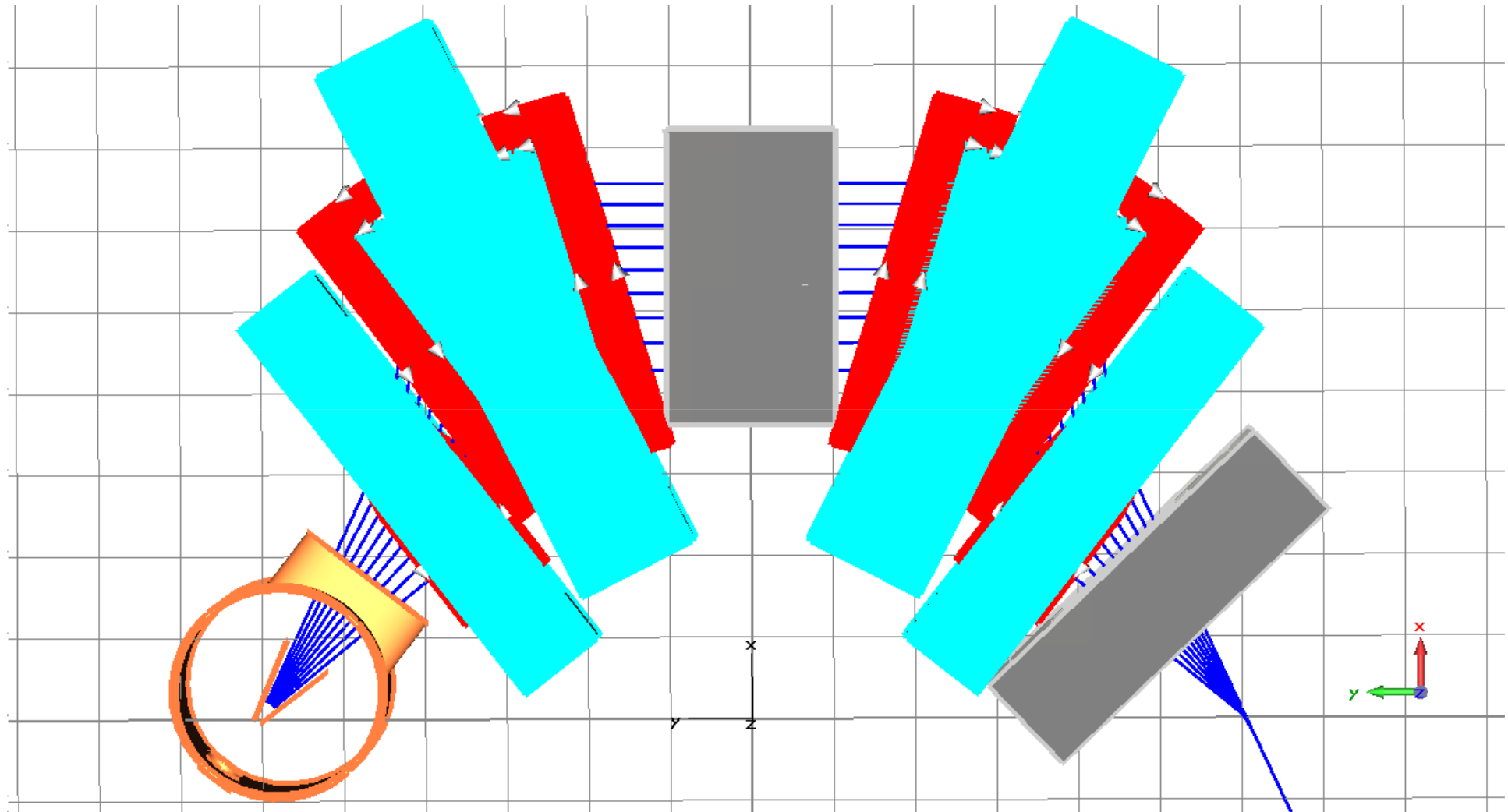
Bunch Compressor: Design / Optimization Cycles



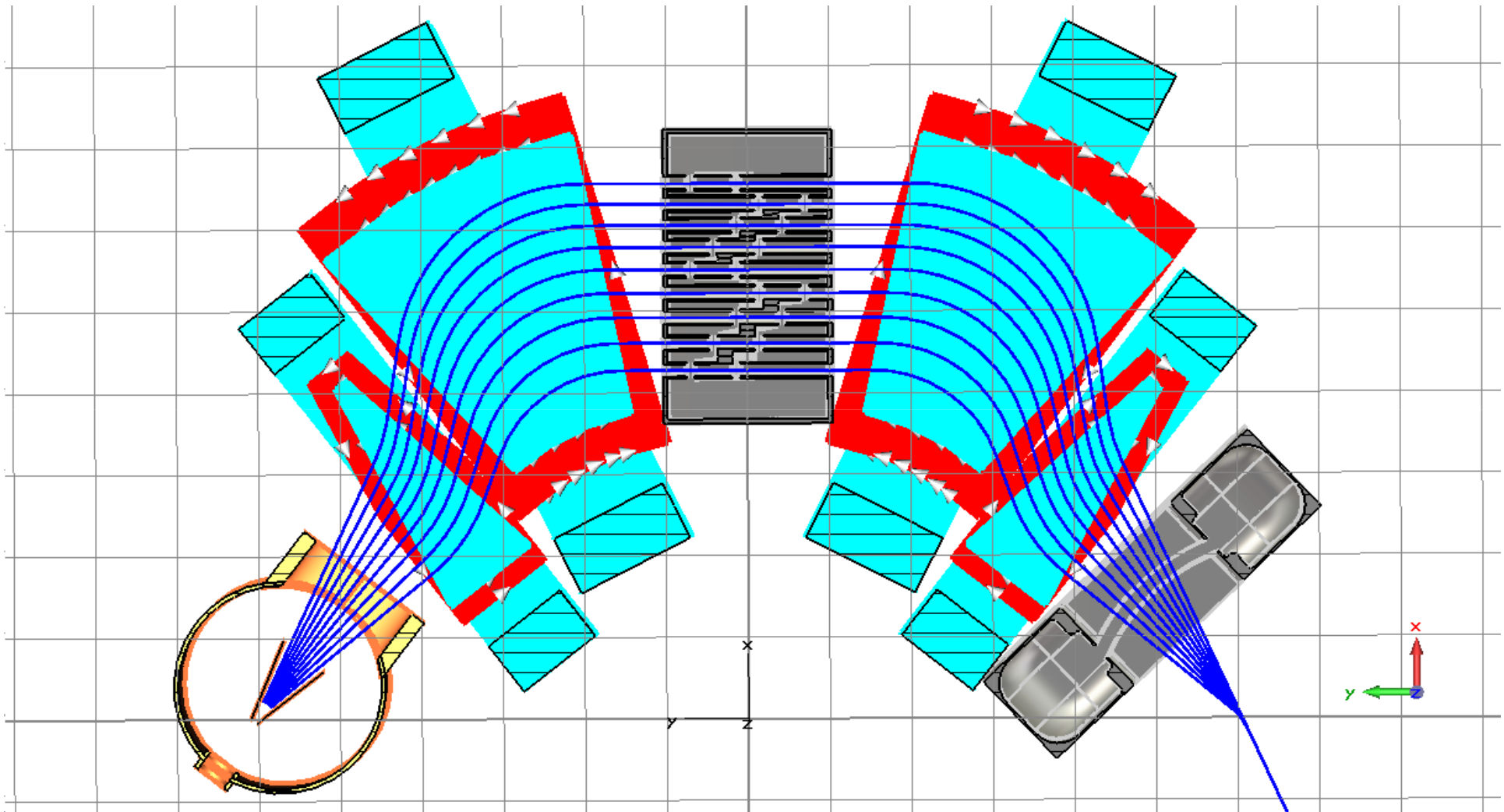
Outlook:

- Improve magnet design, magnet with gradient
- Beam dynamics: Front to end simulation
- Kicker + dipoles + rebunchers + merging scenario

FRANZ: Bunch Compressor

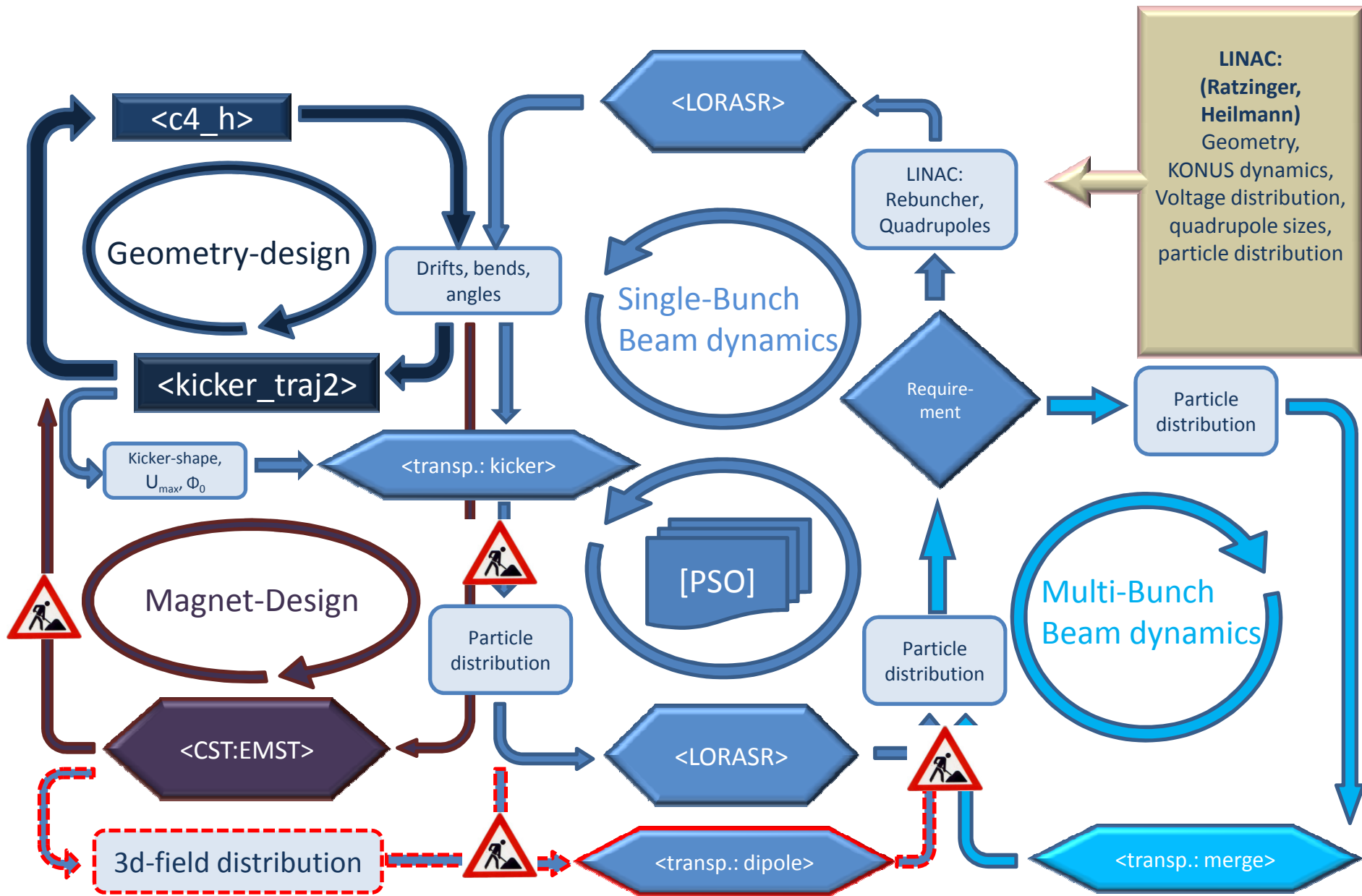


FRANZ: Bunch Compressor

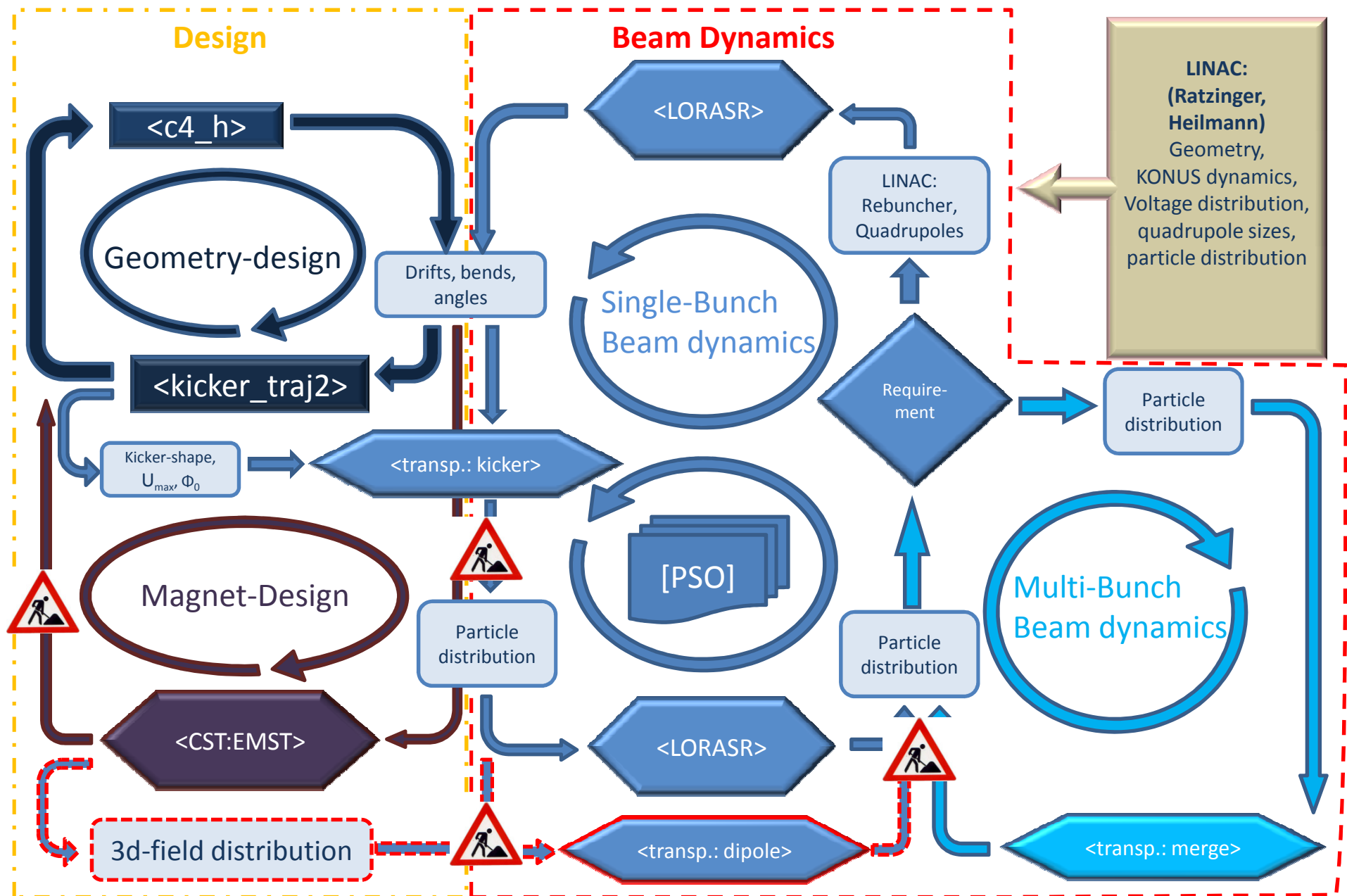


Thank you for your Attention!

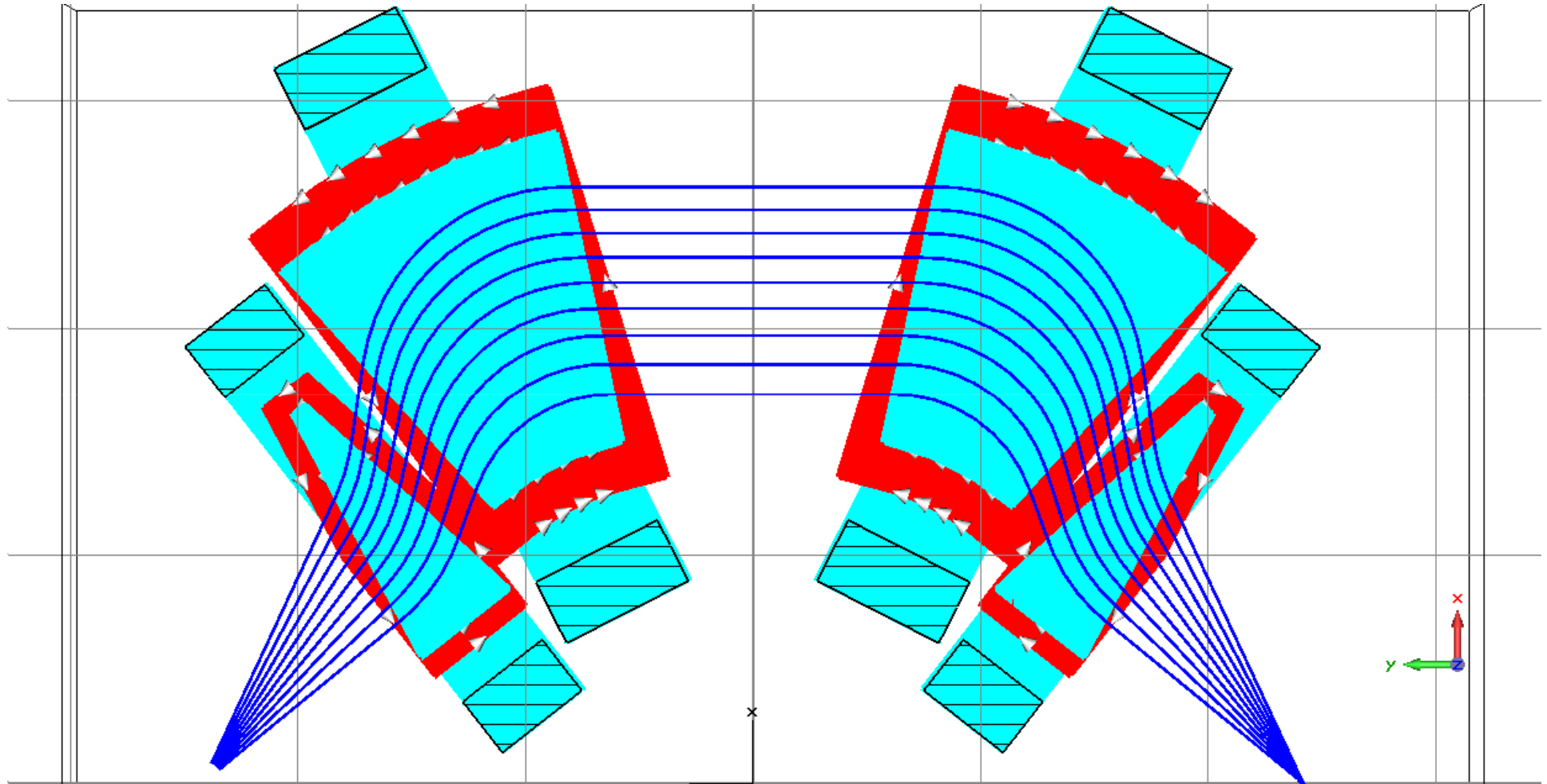
Bunch Compressor: Design / Optimization Cycles



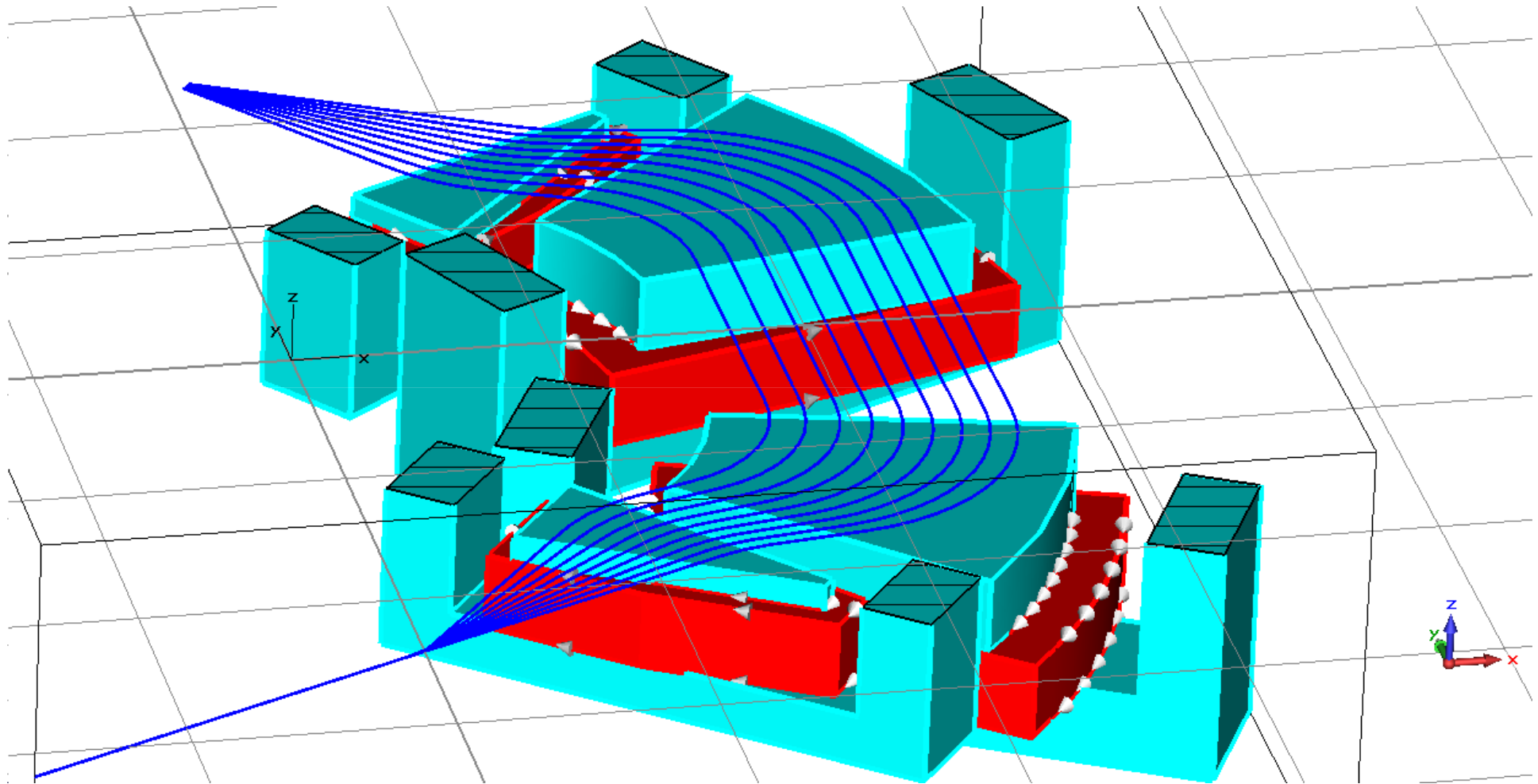
Bunch Compressor: Design / Optimization Cycles



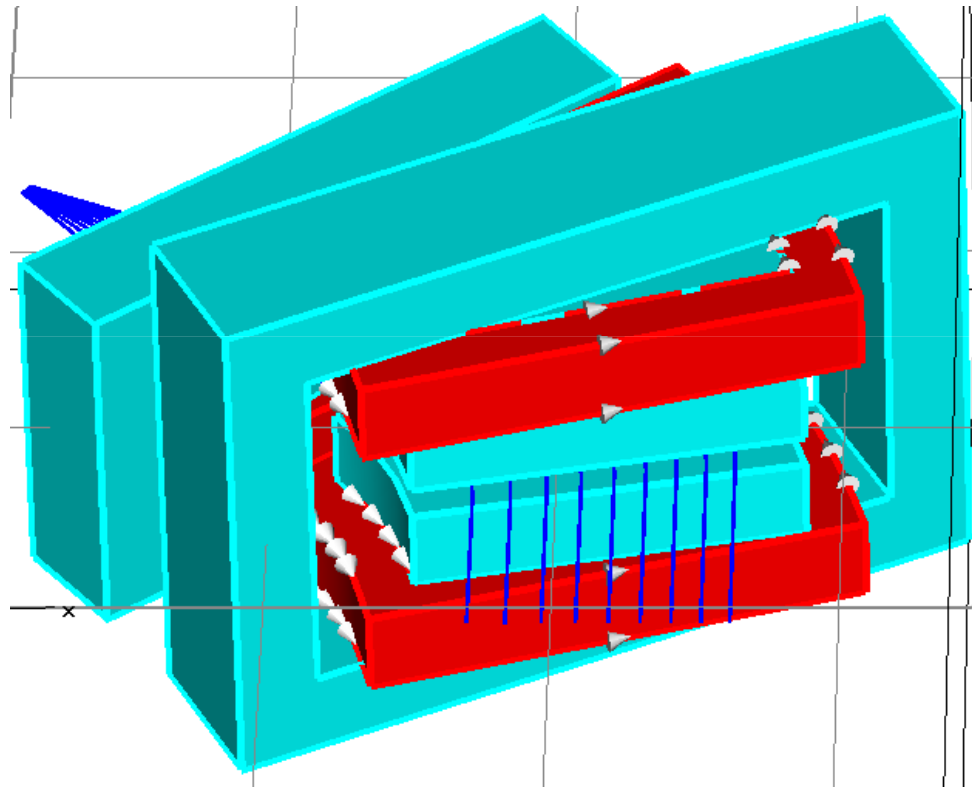
FRANZ: Bunch Compressor



FRANZ: Bunch Compressor

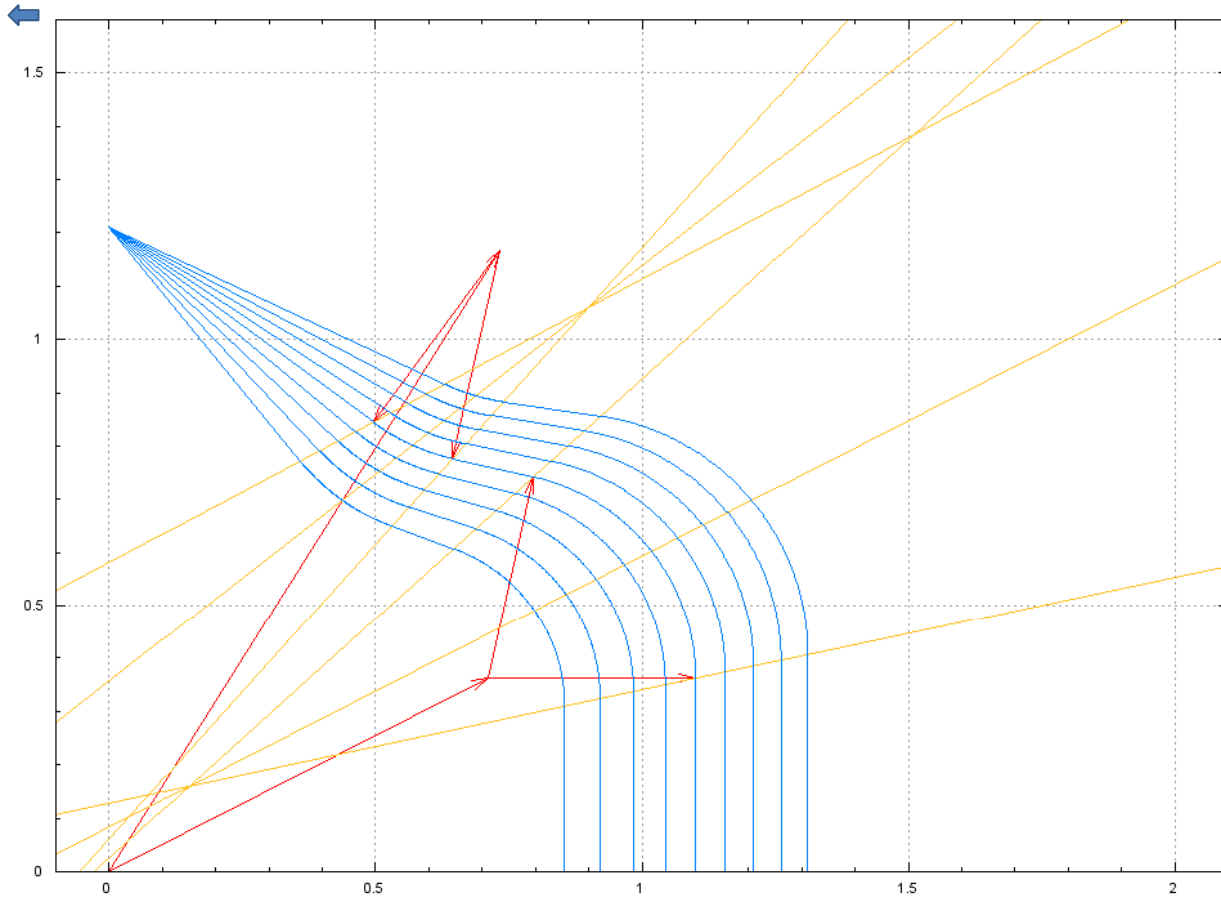


FRANZ: Bunch Compressor



Bunch Compressor: geometrical parameters

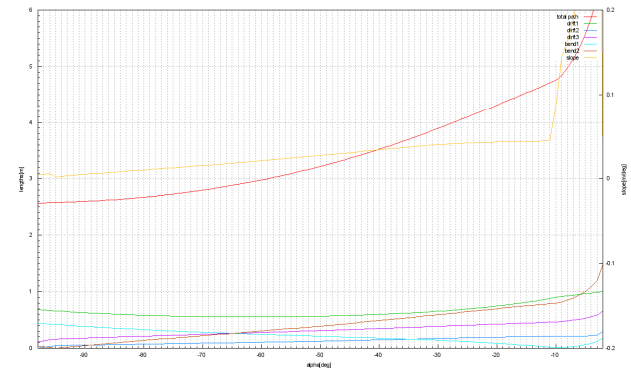
g9_5x



$$B_1 = -0.51497[\text{T}]$$

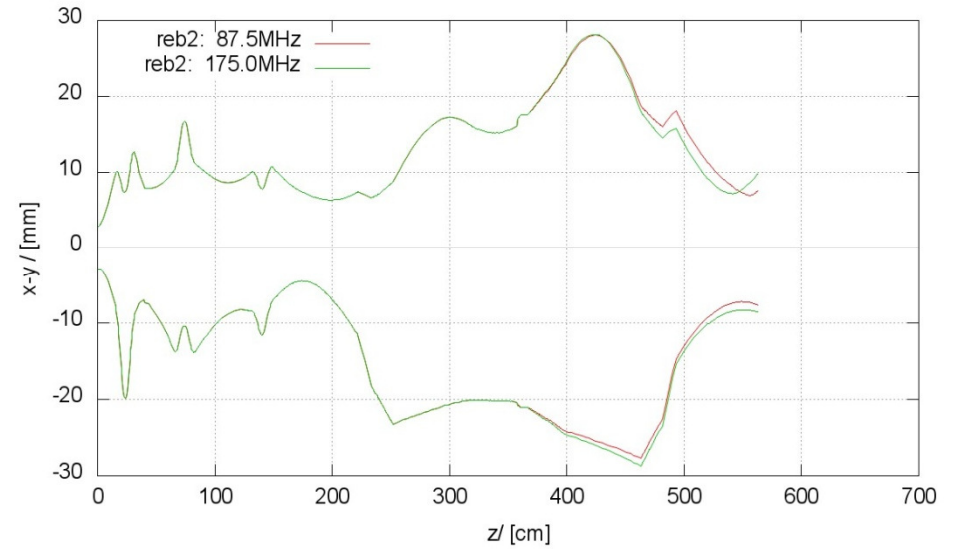
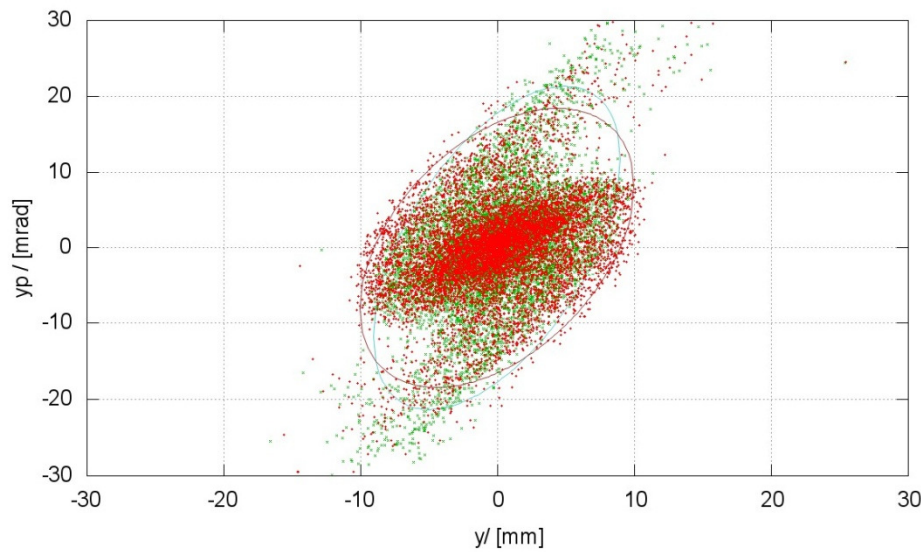
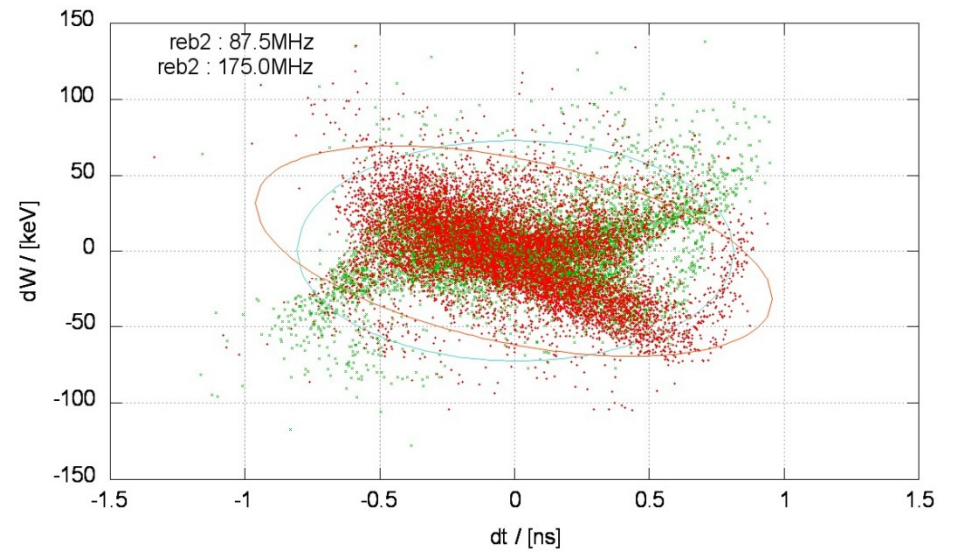
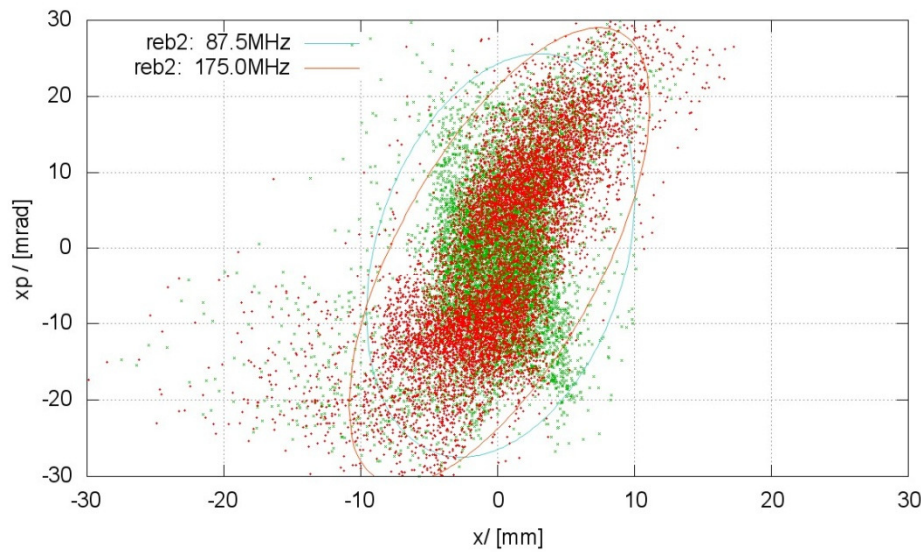
$$\alpha_{\text{max}} = 25.69[\text{deg}]$$

$$\langle \alpha \rangle = 3.21[\text{deg}]$$

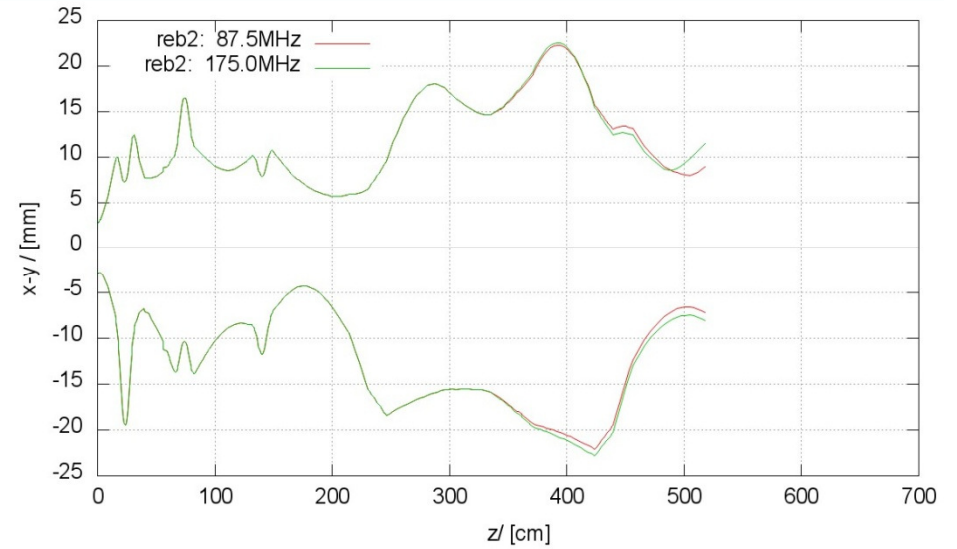
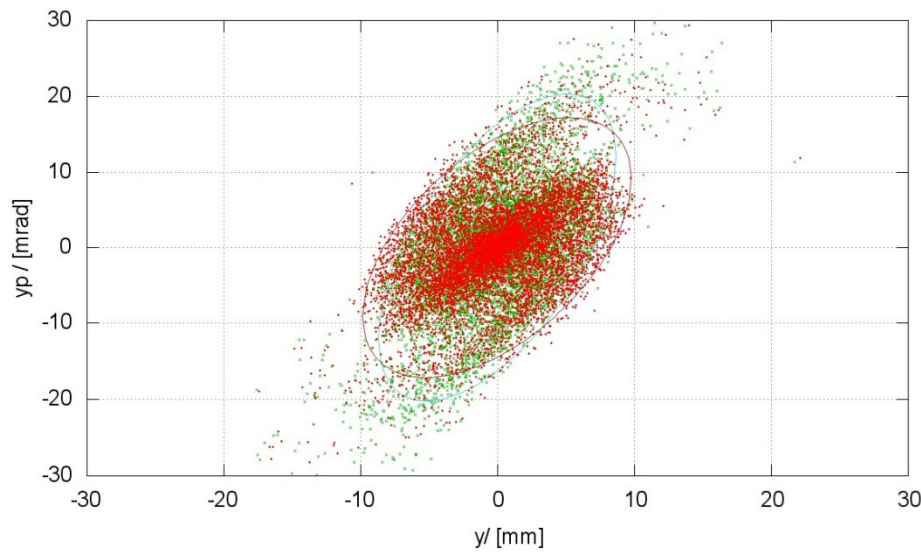
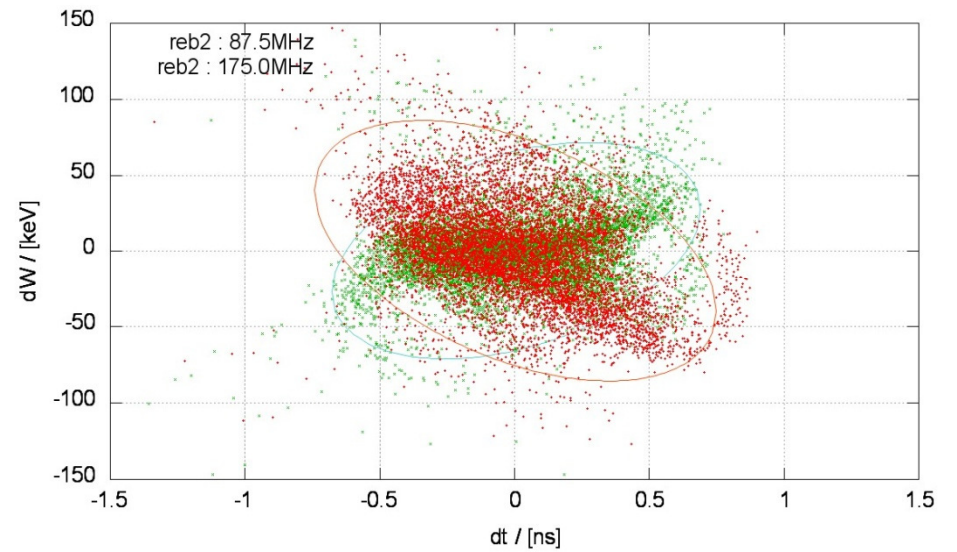
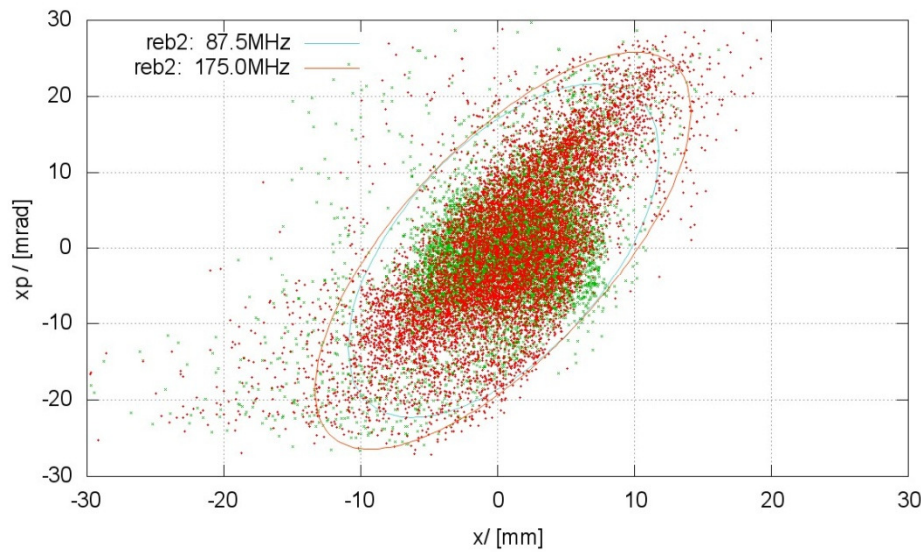


al	tp	dr1	dr2	dr3	b1	b2	bet1	bet2	R2	B2	d_x1	d_x2	d_x3	d_x4	d_x5	d_a	d_x1p	d_tp	psi11	psi12	psi21	psi22
[deg]	[m]	[m]	[m]	[m]	[m]	[m]	[deg]	[deg]	[m]	[T]	[m]	[m]	[m]	[m]	[m]	[deg]	[m]	[m]	[deg]	[deg]	[deg]	[deg]
-25.000	4.0995	0.6949	0.1845	0.4069	0.1162	0.6472	16.645	-81.645	0.4542	0.4535	0.0397	0.0352	0.0412	0.0515	0.0504	2.702	0.0328	-0.1125	37.0000	33.6455	39.6455	12.0000
-27.702	3.9870	0.6718	0.1777	0.3962	0.1296	0.6182	18.560	-80.857	0.4381	0.4702	0.0382	0.0353	0.0419	0.0529	0.0518	2.781	0.0326	-0.1125	34.2979	32.8575	38.8575	12.0000
-30.483	3.8745	0.6510	0.1707	0.3852	0.1421	0.5884	20.349	-79.866	0.4221	0.4880	0.0374	0.0359	0.0429	0.0545	0.0533	2.887	0.0328	-0.1125	31.5167	31.8661	37.8661	12.0000
-33.370	3.7620	0.6323	0.1633	0.3738	0.1540	0.5576	22.052	-78.682	0.4061	0.5073	0.0370	0.0369	0.0442	0.0563	0.0551	3.023	0.0334	-0.1125	28.6298	30.6819	36.6819	12.0000
-36.393	3.6495	0.6154	0.1558	0.3621	0.1655	0.5259	23.703	-77.310	0.3898	0.5285	0.0371	0.0385	0.0461	0.0584	0.0571	3.194	0.0343	-0.1125	25.6071	29.3105	35.3105	12.0000
-39.587	3.5370	0.6003	0.1480	0.3500	0.1769	0.4932	25.339	-75.753	0.3731	0.5522	0.0377	0.0407	0.0485	0.0610	0.0596	3.409	0.0358	-0.1125	22.4131	27.7526	33.7526	12.0000
-42.995	3.4245	0.5870	0.1401	0.3373	0.1885	0.4593	27.001	-74.005	0.3556	0.5793	0.0390	0.0437	0.0516	0.0641	0.0627	3.677	0.0377	-0.1125	19.0046	26.0054	32.0054	12.0000
-46.672	3.3120	0.5754	0.1320	0.3240	0.2006	0.4239	28.735	-72.063	0.3370	0.6112	0.0411	0.0477	0.0557	0.0681	0.0666	4.017	0.0404	-0.1125	15.3277	24.0631	30.0631	12.0000
-50.689	3.1995	0.5660	0.1237	0.3098	0.2137	0.3866	30.607	-69.918	0.3168	0.6502	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0.0000	11.3105	21.9176	27.9176	12.0000

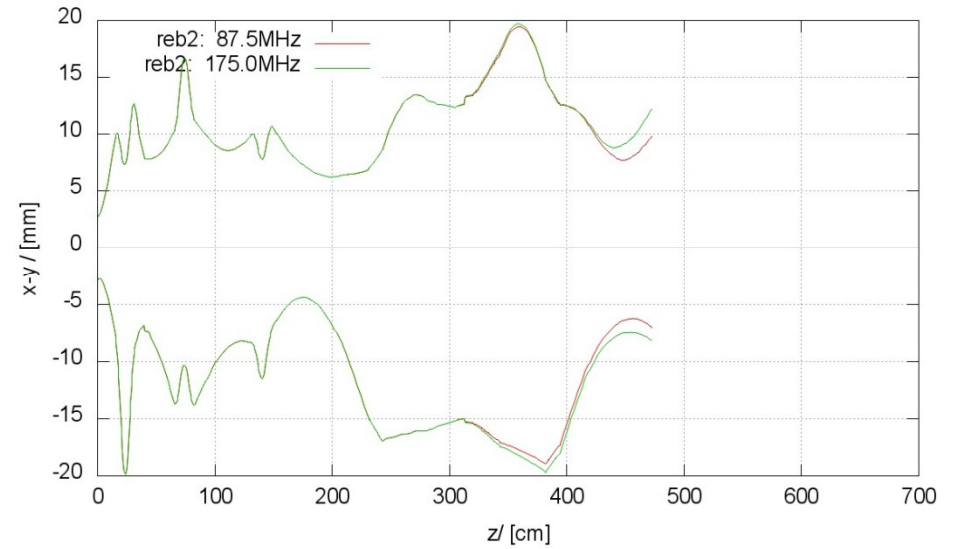
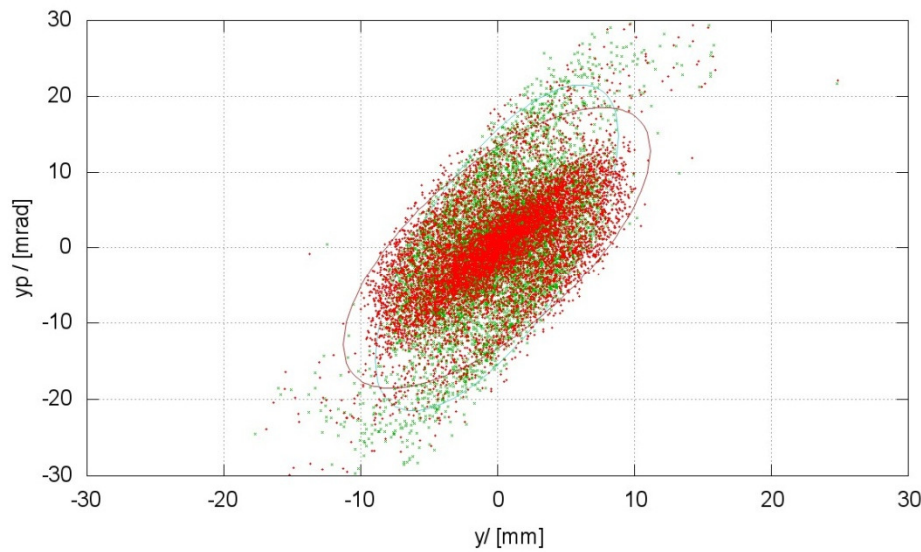
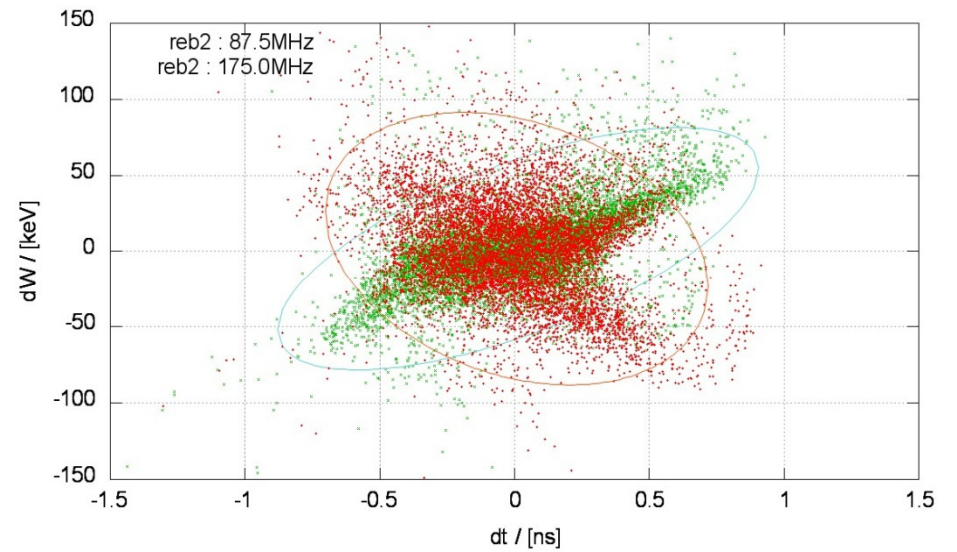
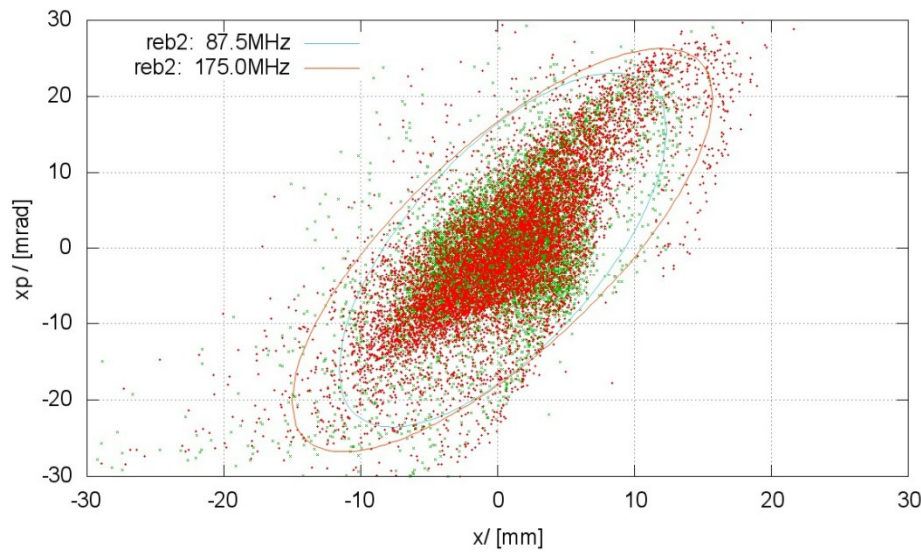
Bunch Compressor: Bunch(1) at the target



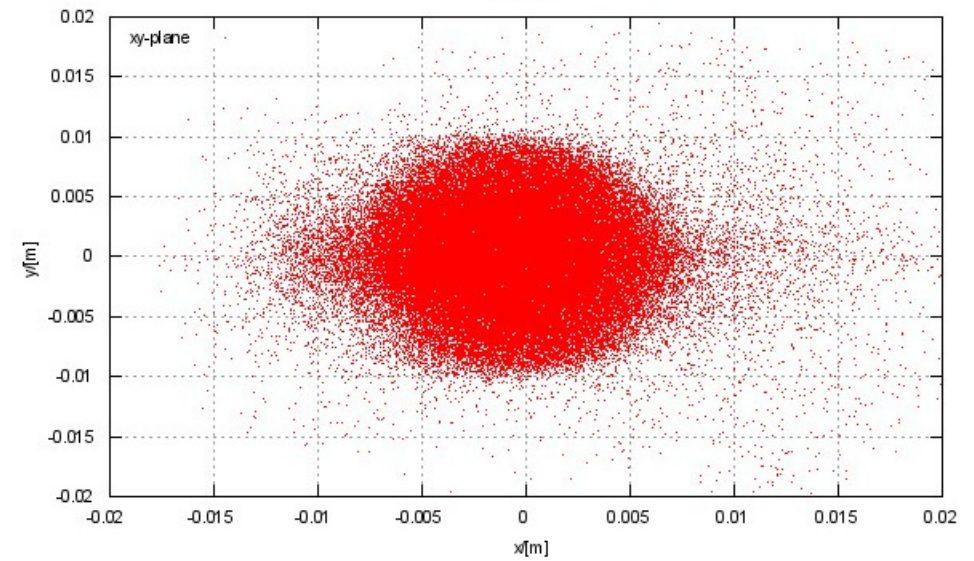
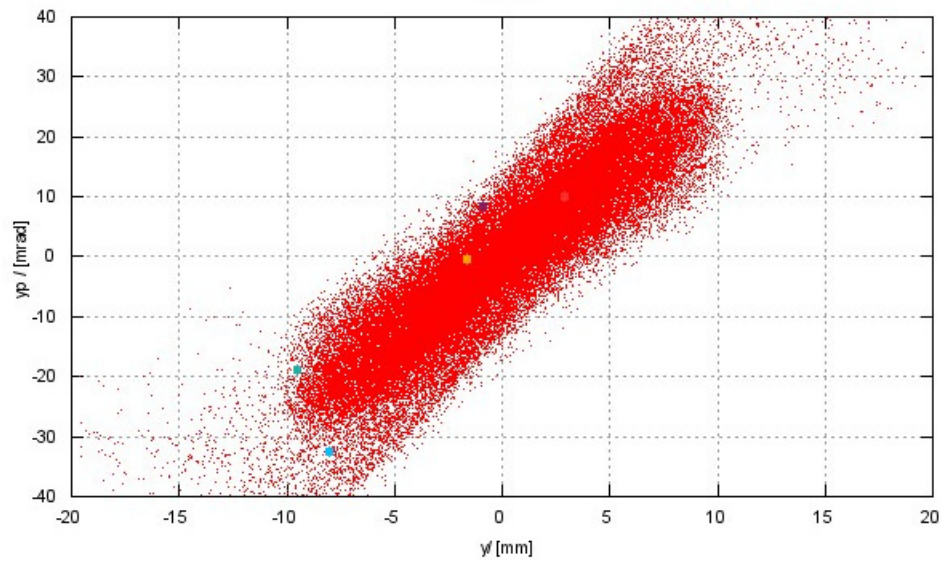
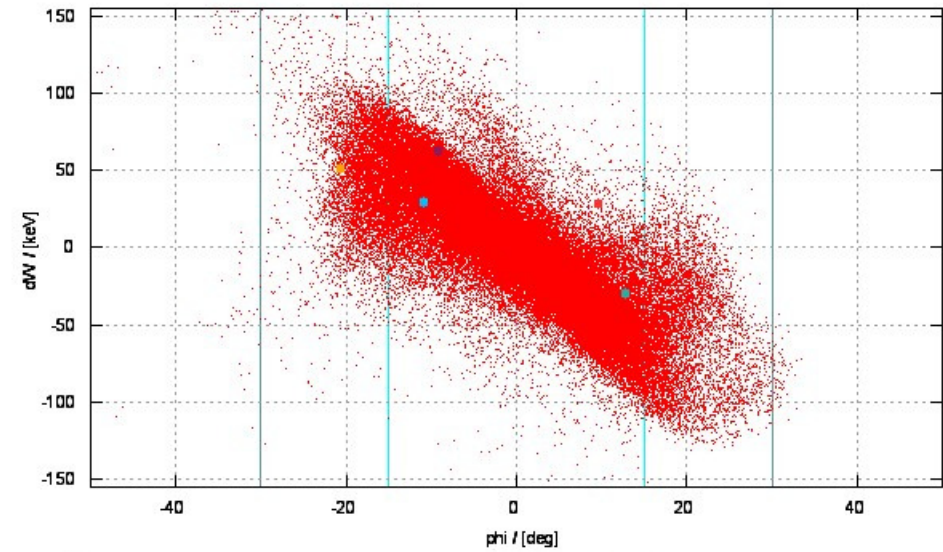
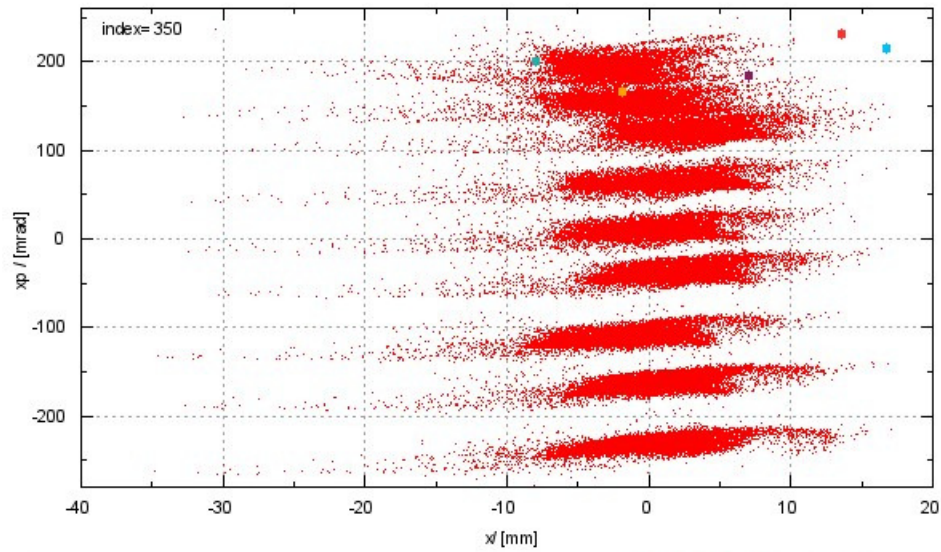
Bunch Compressor: Bunch(5) at the target



Bunch Compressor: Bunch(9) at the target



Bunch Compressor: Merging - Projections at the target





Kantenfokussierung

Beim Durchlaufen der Kante eines Dipols erfahren die Teilchen eine *Impulsänderung* abhängig vom β, g, ρ_0, K und ihrer Positionen (x_0, y_0) bezüglich des Solteilchen.

$$x = x_0 \quad , \quad x' = \Delta x' + x'_0$$

$$y = y_0 \quad , \quad y' = \Delta y' + y'_0$$

radialer Kick: $\Delta x' = + \frac{\tan(\beta)}{\rho_0} \cdot x_0 = k_x \cdot x_0$

axialer Kick: $\Delta y' = - \frac{\tan(\beta_{eff})}{\rho_0} \cdot y_0 = k_y \cdot y_0$

$$\tan(\beta_{eff}) = \tan \beta - \underbrace{\left(\frac{g \cdot K}{\rho_0} \right) \cdot \frac{1 + \sin^2 \beta}{\cos^3 \beta}}_{\text{Korrektur in 1. Ordnung von } \left(\frac{g}{\rho_0} \right)} = \tan \beta - \tilde{K} \cdot \frac{1 + \sin^2 \beta}{\cos^3 \beta}$$

$$\tilde{K} = \frac{g \cdot K}{\rho_0}$$

\tilde{K} => Symmetrie der Abbildung

ρ_0 => Stärke der Abbildung

β = Kantenwinkel

g = Gap

ρ_0 = mittlerer Umlenkradius

K = Randfeld-Integral (später mehr...)

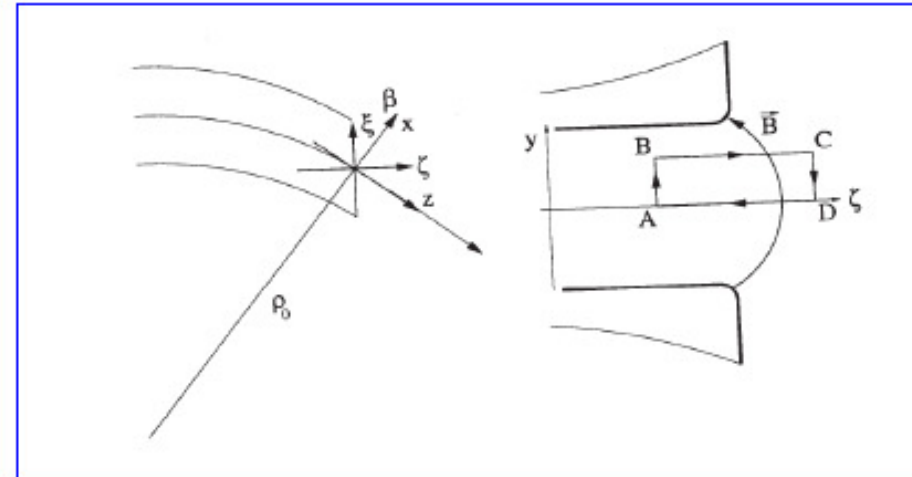


Randfeld-Integral

$$K = \int_A^D d\zeta \frac{1}{g(\zeta)} \frac{B_y(\zeta)}{B_0} \frac{(B_0 - B_y(\zeta))}{B_0}$$

ξ = parallel zur Kante

ζ = senkrecht zur Kante



- Typische Werte für reale Kanten: $K= 0.3 \dots 1.0$, $K=0 \Leftrightarrow$ „hard edge“
- Für $g=\text{const} \Rightarrow K=$ „Maß für die Länge des Randfeld“

je größer K , desto länger ist das Randfelds

- K läßt sich berechnen, wenn die Feldverteilung in ξ -Richtung beispielsweise aus *Meßungen* oder aus *Simulationsprogrammen* bekannt ist