

Status of the Figure-8 Storage Ring F8SR

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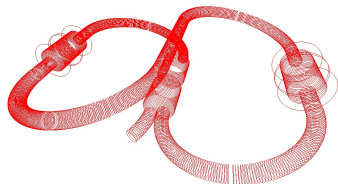
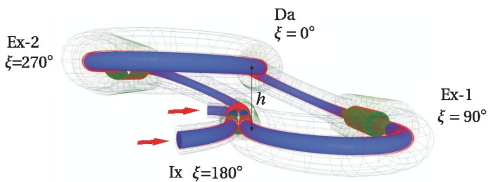
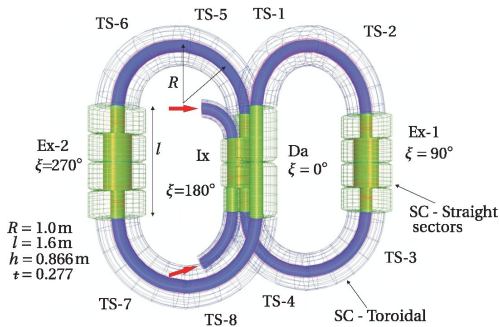
28.02.2014

Outline

- 1 Motivation
- 2 Experiments
 - Setup
 - Momentum-Filter
 - Beam Diagnosis
- 3 Theory & Simulations
 - Closed Orbit Studies
 - Field Imperfections & Error Studies
 - Injection via Adiabatic Compression
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Superconducting High Current Ion Storage Ring F8SR

- Magnetostatic $|\vec{B}| \approx 6 \text{ T}$
- Beam Energy: $W = 150 \text{ keV} - 1 \text{ MeV}$
- Beam Current: $I = 1 - 10 \text{ A}$
- Orbital revolution period: $T = 2 \mu\text{s}$
- Stored Beam Energy & Power:
 $E = 3 \text{ J}$
 $P_{\text{max}} = 1.5 \text{ MW}$



Why to build a new and such crooked Storage Ring - Motivation:

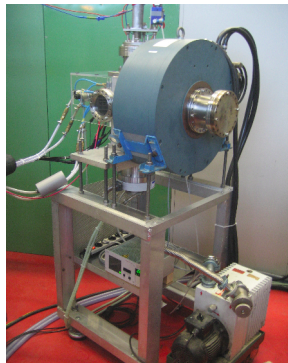
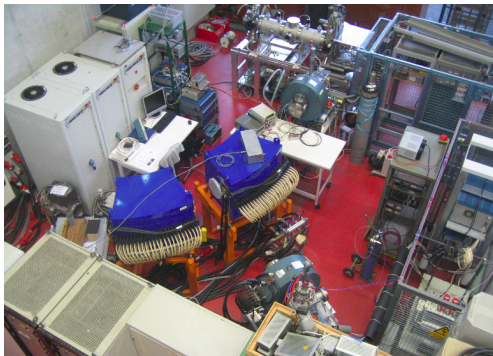
- Fusion reactivity studies in a *High Current Mode* such as
 $p + {}^{11}\text{B} \rightarrow 3 {}^4\text{He} + 8.7 \text{ MeV}$
- multiple beam & particlespecies experiments in *Collider Mode*
down to center of mass collision energies of 100 eV
- space charge compensation by magnetic surface bounded
secondary electrons
- multi ionisation of light atoms by an intense proton beam
- beam plasma interaction
- coulomb screening effects

F8SR Experiments - Setup

Two 30° Toroids, $B_{\max} = 0.6 \text{ T}$

Two refurbished injectors, each with:

- terminal, $U_{\max} = 20 \text{ kV}$
- volume source, $I \approx 3.4 \text{ mA}$ hydrogen mix, max 50% protons
- faraday-cup + solenoid, $B_{\max} = 0.72 \text{ T}$

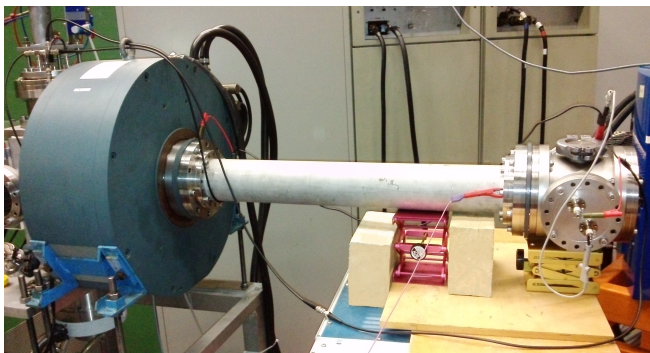


Momentum-Filter

F8SR Experiments - Momentum-Filter

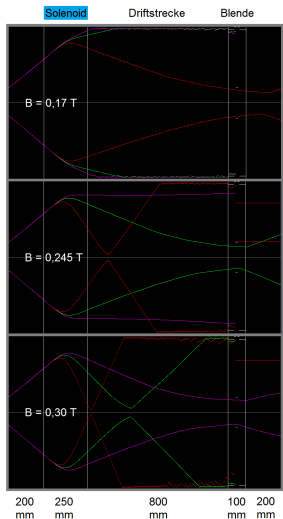
Master Thesis - Heiko Niebuhr:

- Design and construction of a magnetic **Momentum-Filter** for different hydrogen species (H^+ , H_2^+ , H_3^+)



F8SR Experiments - Momentum Filter

Simulations of hydrogen species H^+ , H_2^+ , H_3^+ with LINTRA



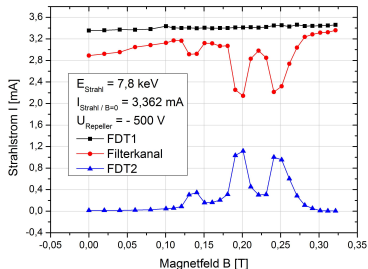
Measurements:

beam current in Faraday-Cups

FDT1: in front of solenoid

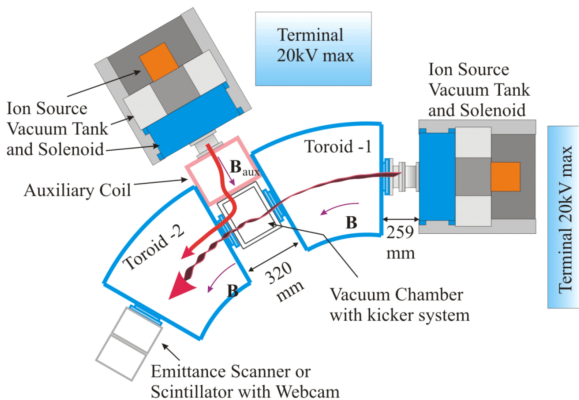
FDT2: behind filter-aperture

filterchannel: grounded via
ampèremeter, $I \sim$ losses



F8SR Experiments - Injection

Injection simulations to determine air-core-coil parameters done (sim.-code *segments*). $B = 0.2 - 0.3 \text{ T}$
 Coil-design and construction is upcoming.

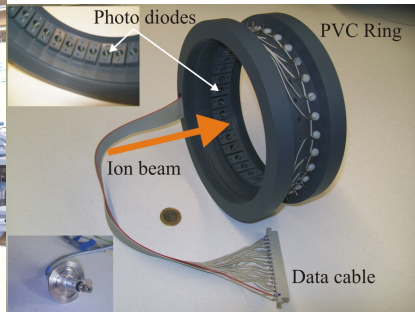


Beam Diagnosis

F8SR Experiments - Diagnosis

Master-Thesis Adem Ates: Non invasive beam diagnosis via residual gas monitor in high magnetic fields

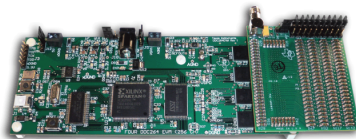
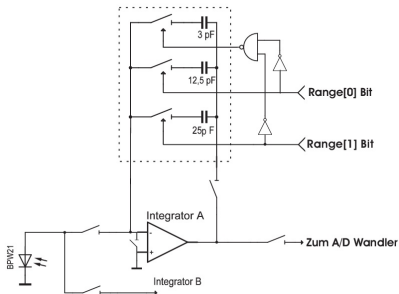
- movable ring of azimuthal photodiodes for visible light



F8SR Experiments - Diagnosis

construction of a rapid recording electronics is done

- 20bit , 256 channels, direct current input & Analog-to-digital converter
- available capacitors: 3pF; 12,5pF; 25pF; 37,5pF ; up to 150pC
- integration times: 160 μ s – 1 s
- input currents: fAs – μ As
- continous measurement via two way input channel

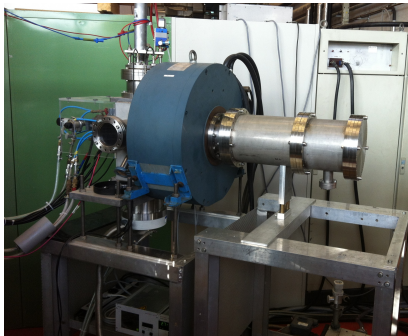


DDC264EVM

F8SR Experiments - Diagnosis

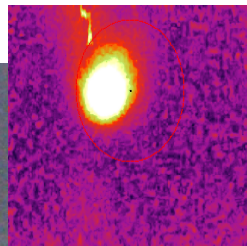
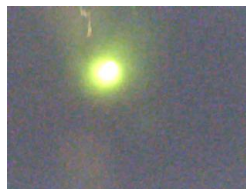
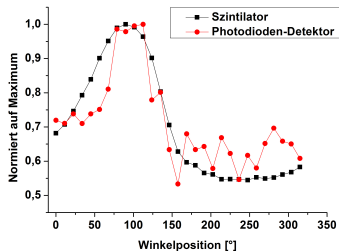
Testing setup:

- extraction voltage: 6.5 kV
- beam current: 1 mA
- solenoid field: 0.33 T
- residual gas pressure: 10^{-5} mbar nitrogen



F8SR Experiments - Diagnosis

- measurement of a He-beam
- comparison with an invasive phosphor screen



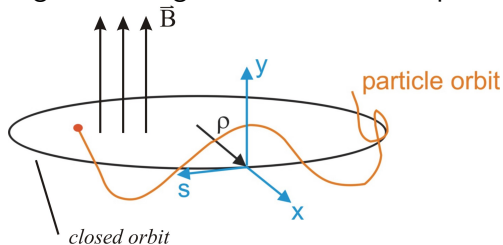
setting up a full diagnosis software with a algorithmical back transformation beam monitoring is the next step

Theory & Simulations

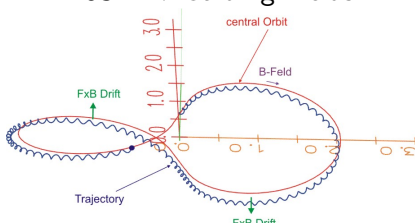
Theory & Simulations

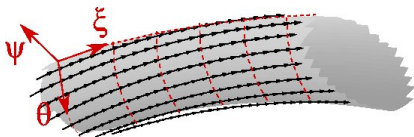
Closed Orbit Studies

Traditional Rings, focussing & corrections → Dipole, Quadrupoles



F8SR → Guiding-Fields





Complex magnetic field geometry inhibits traditional transport description via matrices & fixpoints

→ find analogous description to interlink

In magnetic coordinates (Boozercoordinates) ψ, θ, ξ

→ canonical variables for Drift-Hamiltonian:

$$\theta, P_\theta = \frac{q\psi}{2\pi}$$

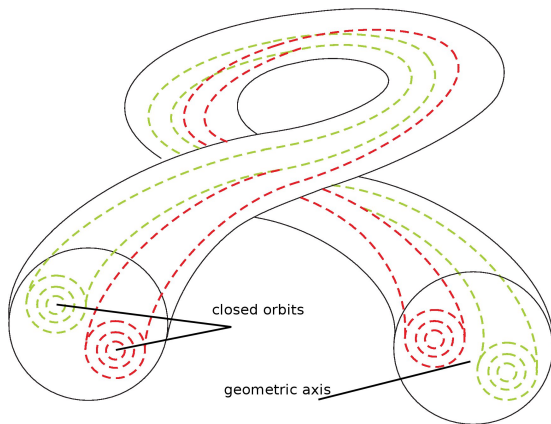
$$\xi, P_\xi = \frac{\mu_0 G}{2\pi|B|} m v_{\parallel} - t \frac{q\psi}{2\pi}$$

$$H = \frac{1}{2m} \frac{(P_\xi + t P_\theta)^2 (2\pi)^2 |B|^2}{\mu_0^2 G^2 m^2} + \mu |B| + q\phi$$

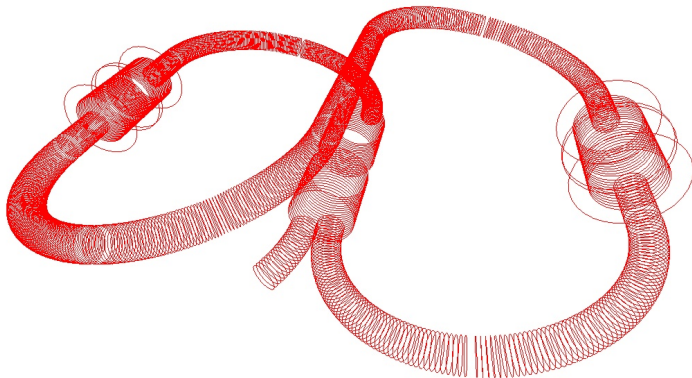
For stable orbits the canonical variables must obey;

$$\begin{aligned} \frac{dP_\theta}{dt} &\stackrel{!}{=} 0 \\ \frac{d\theta}{dt} &\stackrel{!}{=} 0 \\ \frac{dP_\theta}{dt} &= - \left[q \frac{\partial \phi}{\partial \theta} + \left(\mu + \frac{mv_{\parallel}^2}{|\vec{B}|} \right) \frac{\partial |\vec{B}|}{\partial \theta} \right] \\ \frac{d\theta}{dt} &= \frac{2\pi}{q} \left[q \frac{\partial \phi}{\partial \psi} + \left(\mu + \frac{mv_{\parallel}^2}{|\vec{B}|} \right) \frac{\partial |\vec{B}|}{\partial \psi} \right] + t \frac{d\xi}{dt} \end{aligned}$$

- fixpoint studies with multipole expansion within the fieldmap are ongoing
- conventional 2d multipole expansion investigations do not satisfy the complex field geometry



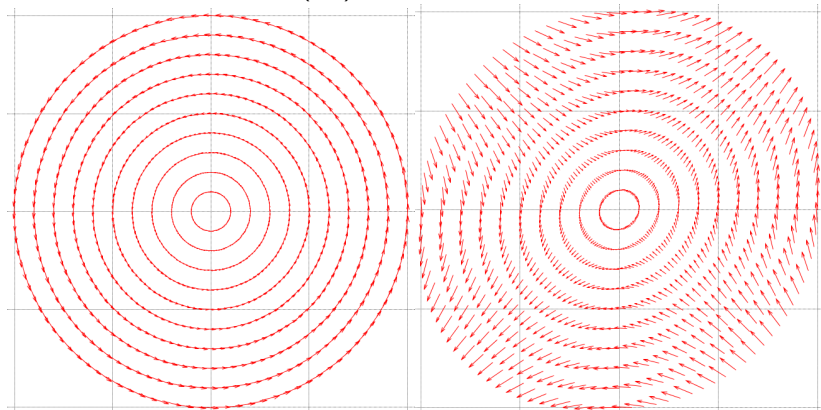
Field Imperfections & Error Studies



Construction always has coil missalignment → interfering multipole fields

Since \vec{B} has components: $B_\psi = 0$, B_ξ , B_θ

Superposing a **poloidal** (B_θ) and **multipole** field. What do we get?



$$\vec{B} = \vec{B}_\theta + \vec{B}_{\text{quad}}$$

$$\vec{B}_\theta = \hat{B}_\theta \begin{pmatrix} -\sin \theta \\ \cos \theta \end{pmatrix} \quad \vec{B}_{\text{quad}} = \frac{\hat{B}_q r}{a} \begin{pmatrix} \sin \theta \\ \cos \theta \end{pmatrix}$$

One obtains points with $|B| = 0 \rightarrow$ analytically solvable:

superposed **quadrupole**:

$$\left\{ \theta = \frac{\pi}{2}, \quad r = \frac{\hat{B}_\theta}{\hat{B}_q} a \right\}; \left\{ \theta = \frac{3\pi}{2}, \quad r = \frac{\hat{B}_\theta}{\hat{B}_q} a \right\}$$

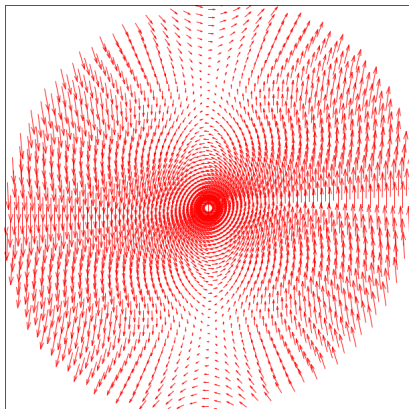
superposed **sextupole**:

$$\left\{ \theta = \frac{\pi}{3}, \quad r = \sqrt{\frac{\hat{B}_\theta}{\hat{B}_q}} a \right\}; \left\{ \theta = \pi, \quad r = \sqrt{\frac{\hat{B}_\theta}{\hat{B}_q}} a \right\}; \left\{ \theta = \frac{5\pi}{3}, \quad r = \sqrt{\frac{\hat{B}_\theta}{\hat{B}_q}} a \right\}$$

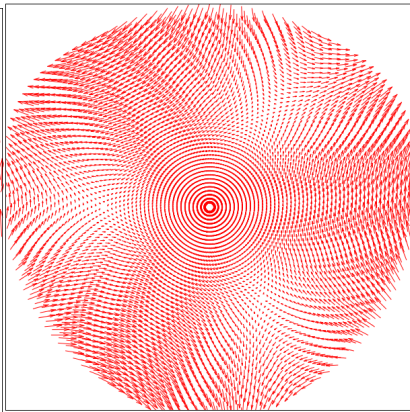
poloidal + quadrupole

→ Quadrupoles around $|B| = 0$

Poloidal around center area

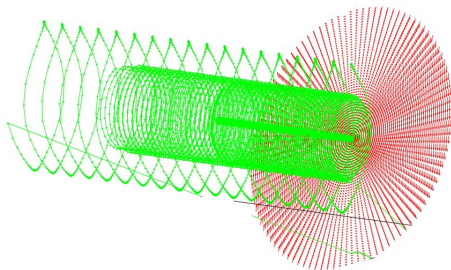
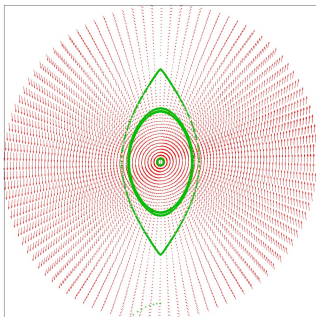


poloidal + sextupole

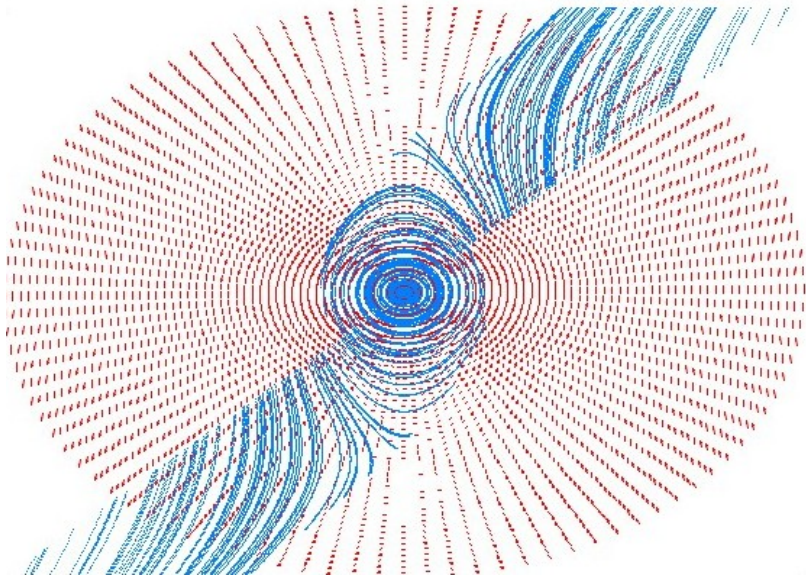


Influence on particle transport?

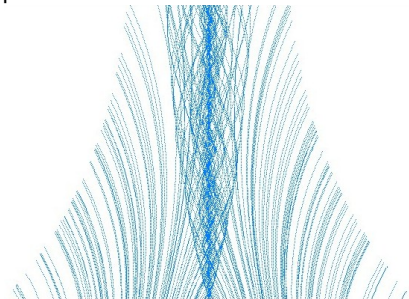
Simulations with $\hat{B}_\theta = \hat{B}_q = 0.1\% \hat{B}_\xi$



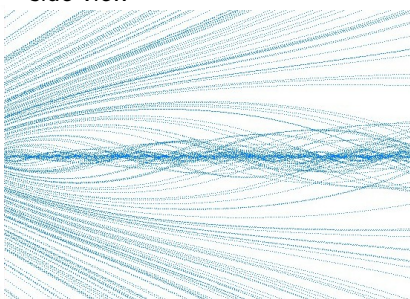
front view



top view



side view



→ certain aperture at a specific slice

→ dynamic aperture along the ring axis

Acceptance of the confinement area is reduced

→ areas of particle loss

Injection via Adiabatic Compression

Injection via Adiabatic Compression

Concerning the canonical momentum

$$\vec{p} = m\vec{v} + q\vec{A}$$

even if $\vec{v} \parallel \vec{B}$ at injection point

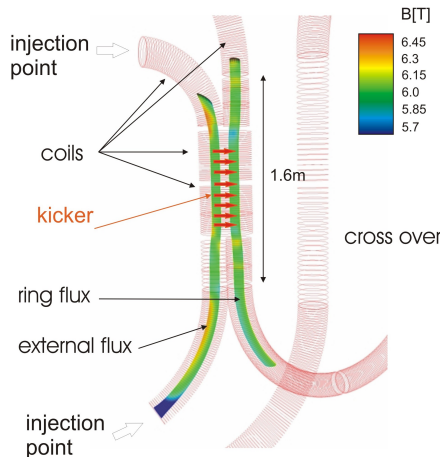
one obtain

$\Delta\vec{A} \rightarrow \Delta\vec{v}$ during entering

\rightarrow radius of acceptance

$$r = \frac{2mv_{\parallel}}{qB}$$

$$r|_{B=6\text{T}} = 8\text{ mm}$$

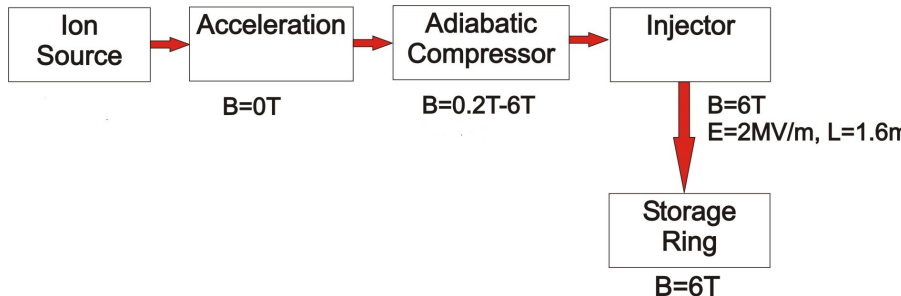


Injection via Adiabatic Compression

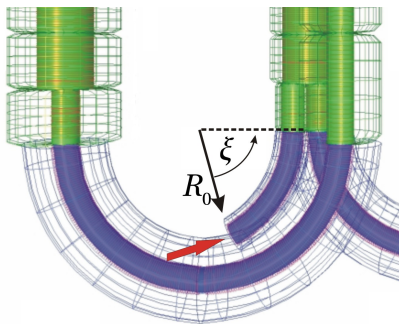
- the facing problem is a smooth field transition

magnetic moment $\mu = \frac{mv_{\perp}^2}{2B}$ must be constant
 → adiabatic invariant

$$\frac{dB}{dt} = \frac{\partial B}{\partial t} + v_z \frac{\partial B}{\partial z} < B \frac{\omega_c}{2\pi} = \frac{qB^2}{2\pi m} \rightarrow v_z \frac{\Delta B}{\Delta z} < q \frac{B^2}{2\pi m}$$

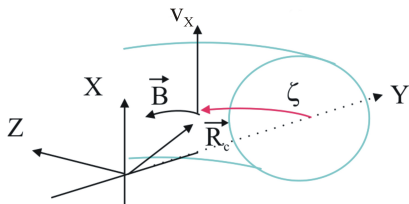


Injection via Adiabatic Compression



due to the gradient $\frac{\Delta B}{\Delta s} \rightarrow B(x, y, z) \rightarrow B(\xi)$

Injection via Adiabatic Compression



$$\vec{v}_d = \frac{1}{q} \frac{\vec{F} \times \vec{B}}{B^2} \quad \vec{F}_c = \frac{mv_{\parallel}^2}{R_c} \rightarrow \vec{v}_d = \frac{mv_{\parallel}^2}{qB^2} \frac{\vec{R}_c \times \vec{B}}{R_c^2}$$

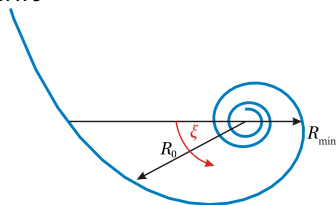
drift velocity coming from $R \times B$ drift

$$V_x = \frac{mv_{\parallel}^2}{qB(\xi)R}$$

$$v_x \stackrel{!}{=} \text{const.}$$

$$\rightarrow B(\xi) \cdot R(\xi) \stackrel{!}{=} \text{const.}$$

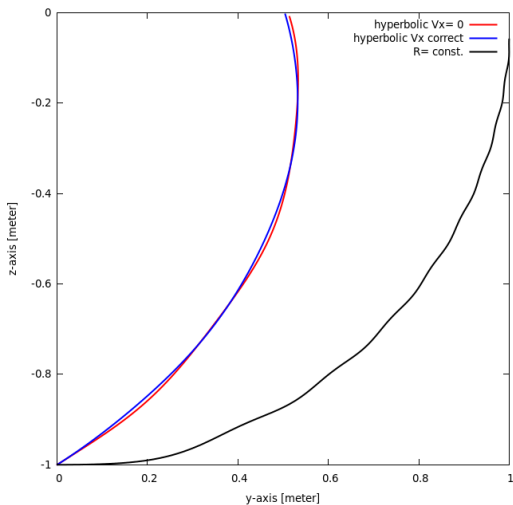
$$B(\xi) = a_1 \cdot \xi \quad R(\xi) = a_2 \cdot \frac{1}{\xi}$$



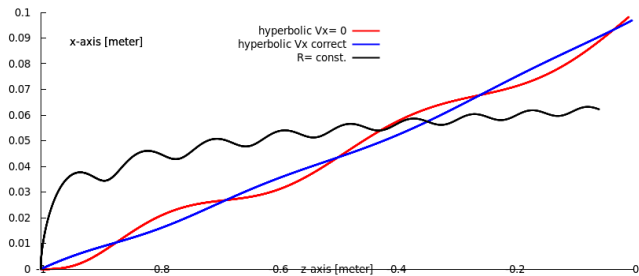
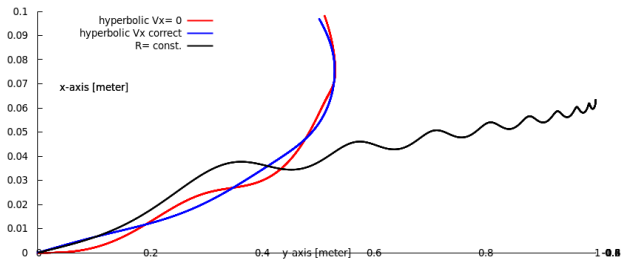
hyperbolic spiral transport channel

Injection via Adiabatic Compression

Single particle simulations, $\vec{v} = \vec{v}_x + \vec{v}_{||}$



Injection via Adiabatic Compression



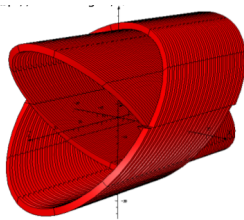
Injection via Adiabatic Compression

Another possible solution to compensate the drift is by adding a dipole component

$$x(\theta) = R \cdot \cos(\theta)$$

$$y(\theta) = R \cdot \sin(\theta)$$

$$z(\theta) = \frac{h\theta}{2\pi} + \frac{R}{\tan \alpha} \sin(n\theta + \varphi_0)$$



[S.Sheehy, BeamDynamicsMeetsMagnets 2013]

→ to be investigated

Outlook

- commissioning of the injection experiment when the coil is ready
- design of the adiabatic injection section for the latest F8SR type
- high current beam transport simulations
- target fusion cross section simulations

Thank you for listening!



Fixpoints & Multipole expansion

Choose a certain point as a possible fixpoint

→ interpolate the field at points on concentric circles

$$\vec{B}_{\text{res}} = \vec{B}_{\perp} - \vec{B}_{\perp,0}$$

where $\vec{B}_{\perp} = B^{\theta} \vec{e}_{\theta}$

→ start multipole expansion

$$C_n = \frac{1}{Mr_0^{n-1}} \sum_{m=1}^M (B_y + iB_x)_m e^{-i\phi_m(n-1)}$$

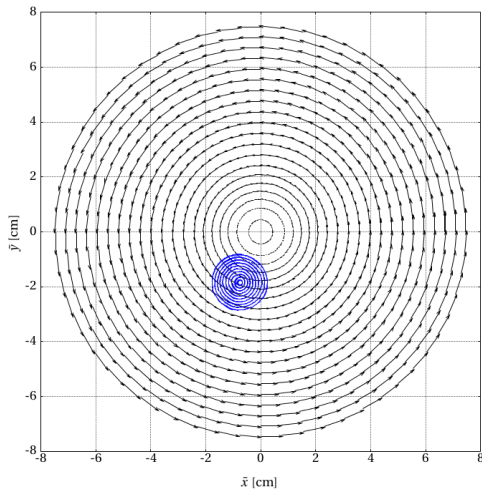
where	$n =$	dipole 1	quadrupole 2	sextupole 3	...
					...

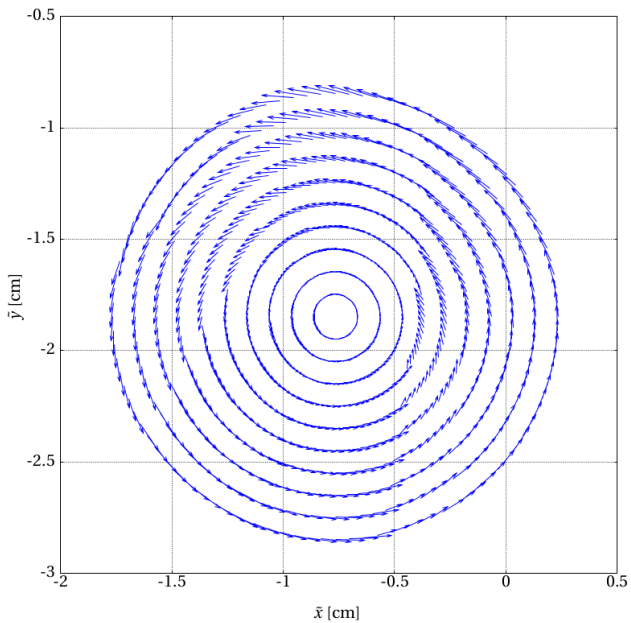
For a poloidal field $\vec{B} = B \begin{pmatrix} -\sin \theta \\ \cos \theta \end{pmatrix}$ one gets $C_n = 0 \quad \forall n$

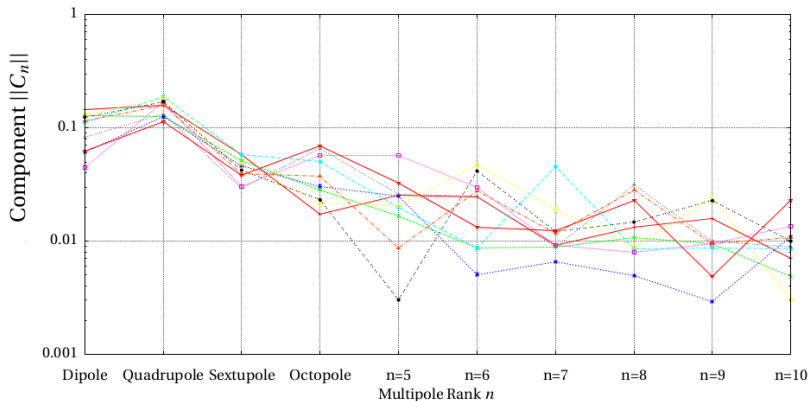
Slice of the mesh ("beam tube")

black = \vec{B}_θ component

blue: \vec{B}_{res}







→ small or almost none amount of multipole components
 problem: this kind of multipole expansion lacks 3rd dimension
 $B^\theta \vec{e}_\theta$ is just a projection $3d \rightarrow 2d$